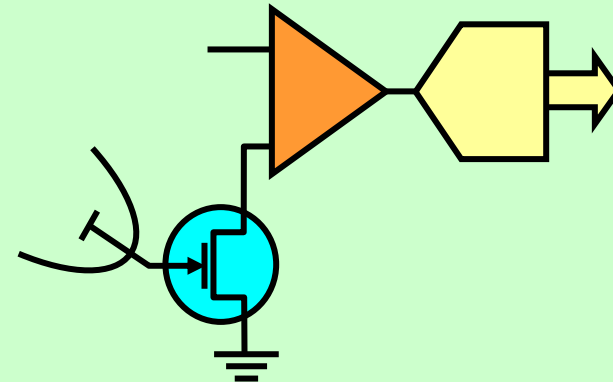
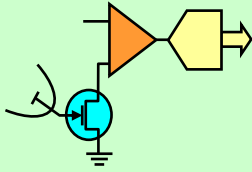


Analog and Telecommunication Electronics

C5 - Synchronous demodulation

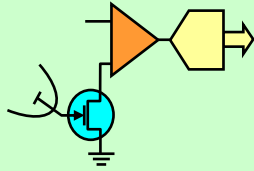
- » AM and FM demodulation
- » Coherent demodulation
- » Tone decoders





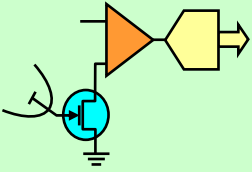
Lesson C5: synchronous demod.

- FM demodulators
- AM demodulators
 - Envelope and
 - Synchronous demodulators
- Digital modulations
 - FSK, PSK, ASK and others
- Tone decoders
 - NE 567 block diagram and parameters
- References sect. 3.7.1, 3.7.2

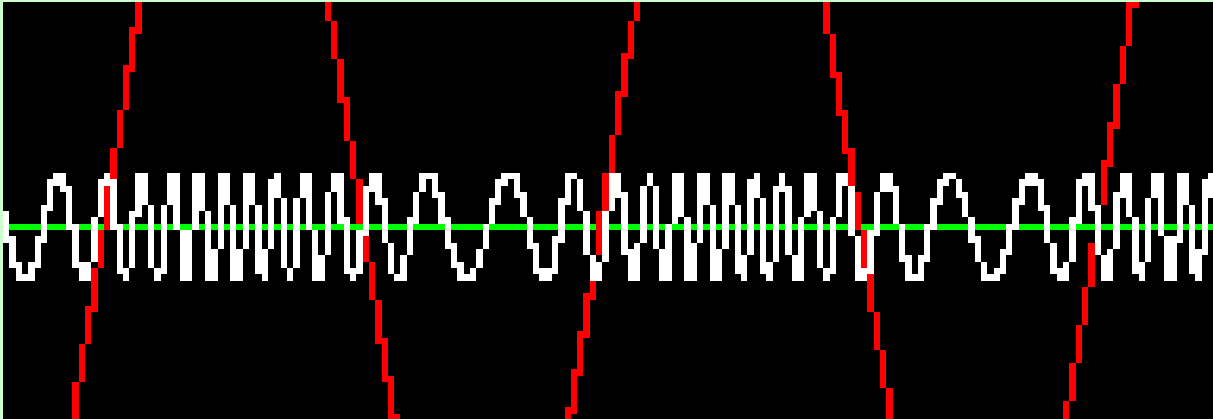


FM mo-demodulation

- Carrier frequency F_p , modulating signal $M(t)$
 - $F_p = F_{p0} + K M(t)$
 - Actual spectrum related with K
- Demodulation:
 - Techniques derived from AM
 - » Change FM into AM
 - » Use AM demodulator
 - PLL-based technique
 - » F_p must be in the lock range
 - » $M(t)$ proportional to $V_c(t)$

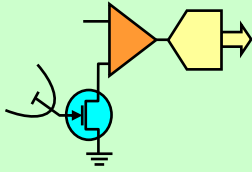


Analog FM example



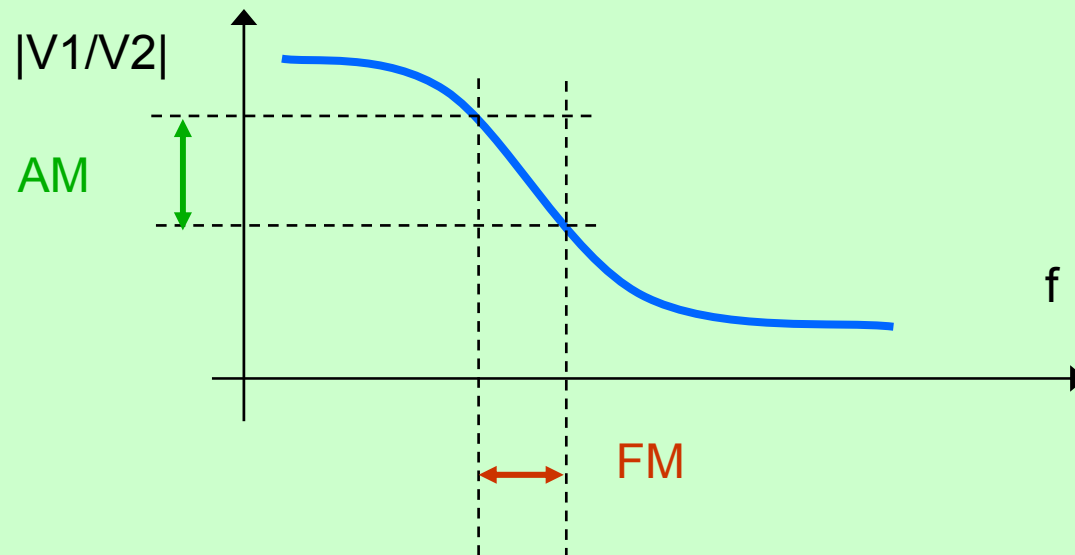
- Red: modulating signal
- White: FM signal

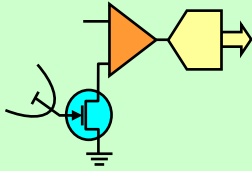
Add spectrum



FM → AM demodulation

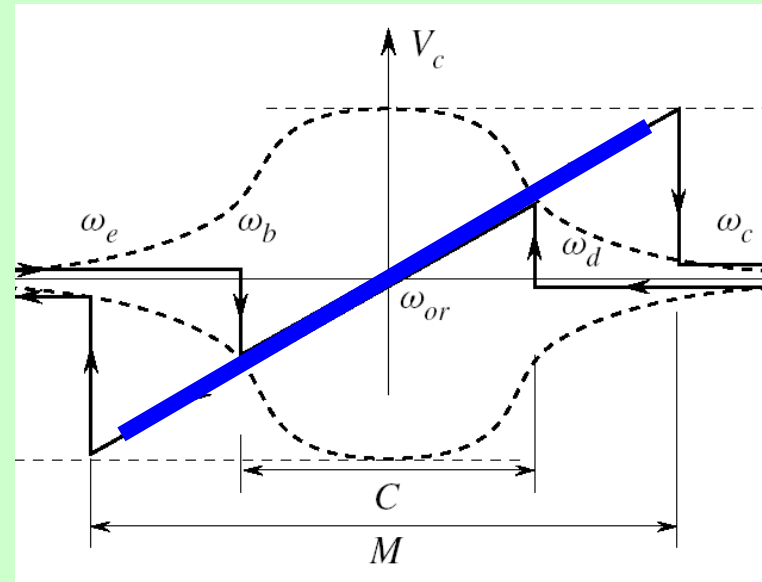
- Exploit the transition region of a steep filter
 - Frequency changes become amplitude changes

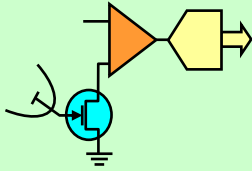




FM PLL demodulation

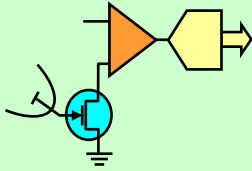
- $F_p = F_{po} + K M(t)$
- PLL locked
 - Full F_p spectrum in the lock range
 - $V_c(t)$ proportional to $M(t)$





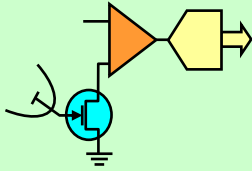
Lesson B5: synchronous demod.

- FM demodulators
- AM demodulators
 - Envelope demodulators
 - Synchronous demodulators
- Digital modulations
 - FSK, PSK, ASK and others
- Tone decoders
 - NE 567 block diagram and parameters



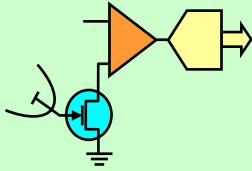
AM signals

- Modulation:
 - Multiplication of carrier $P(F_p)$ by modulating signal M
 - » $S = F_p \times M$
 - » Time domain: M is the envelope of $S(t)$
 - » Frequency domain: M spectrum $M(0)$ translated to $M(F_p)$
- Demodulation
 - Obtain envelope:
 - » Half- or full-wave rectifier + LPF
 - Move S to baseband (spectral translation)
 - » Coherent demodulation
 - » Needs reference signal: PLL



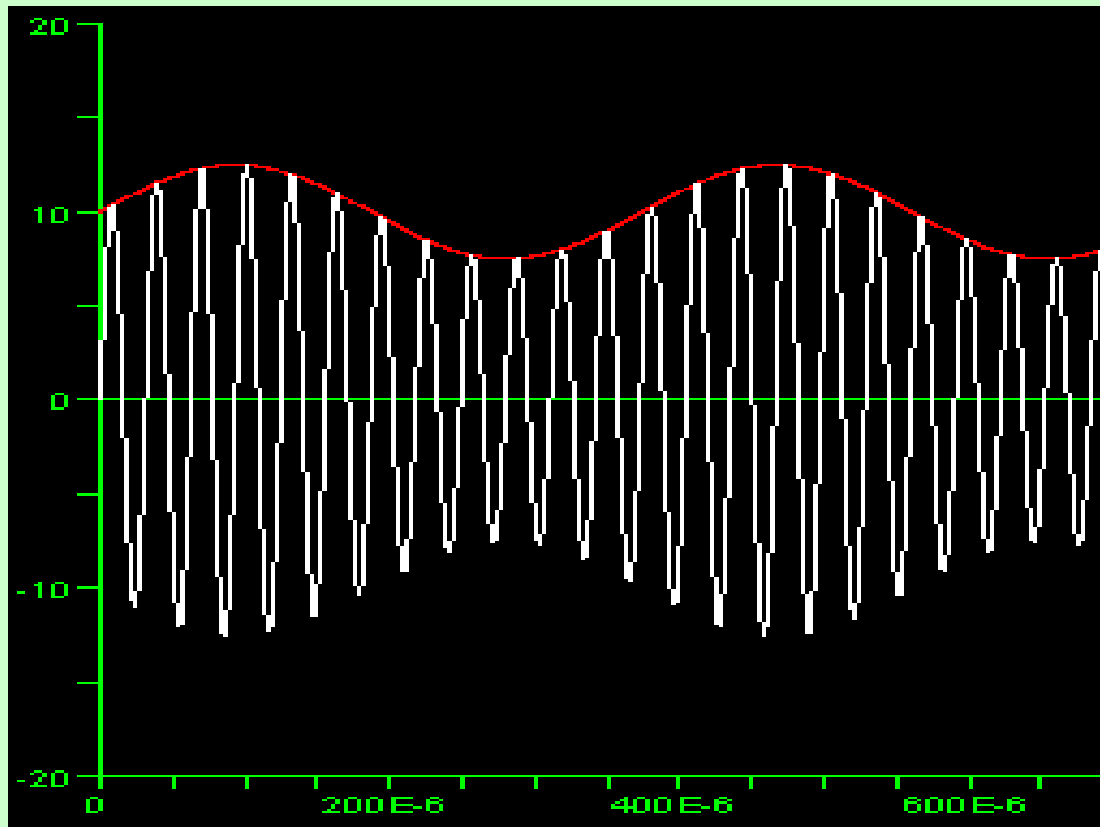
Examples of AM signals

- AM modulation
 - Modulating signal: $A \sin \omega t + B$
 - » max: $A+B$, min: $B-A$
 - » Modulation index m
 $m = (\max - \min) / (\max + \min) = A/B$
 - » $m = 1$: $A = B$ (DC = V_p)
 - Examples with simulator
 - » AM 25% ($m = 0,25$)
 - » AM 50% ($m = 0,5$)
 - » AM 100% ($m = 1$)
 - » AM 200% (PSK-180°, DSB – suppressed carrier)

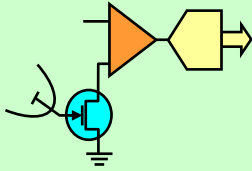


AM modulation: $m = 0,25$

- $A = 2,5V$, $B = 10 V$, $m = 0,25$ (25%)

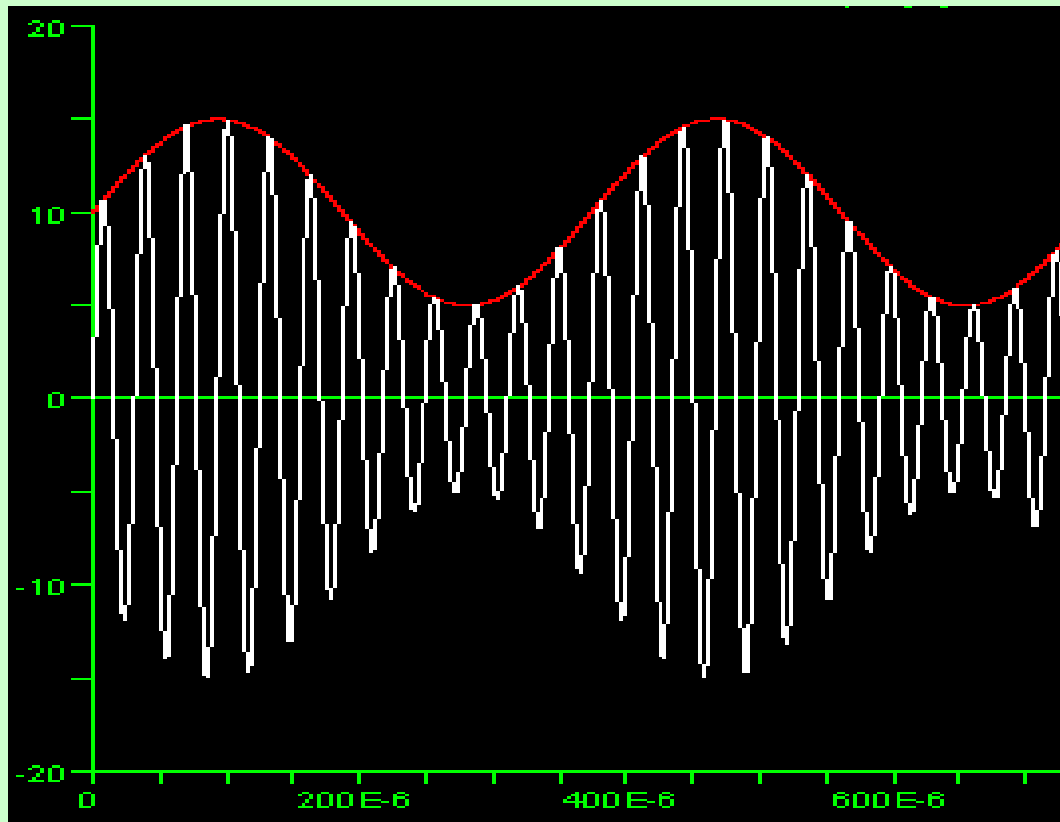


spectrum

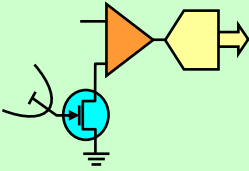


AM modulation: $m = 0,5$

- $A = 5V$, $B = 10 V$, $m = 0,5$ (50%)

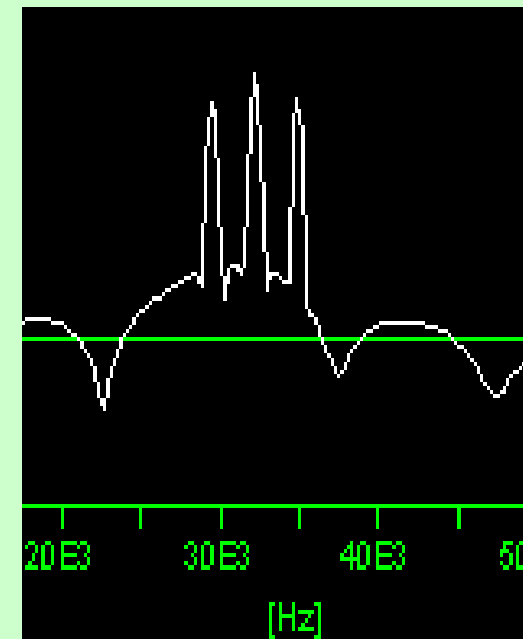
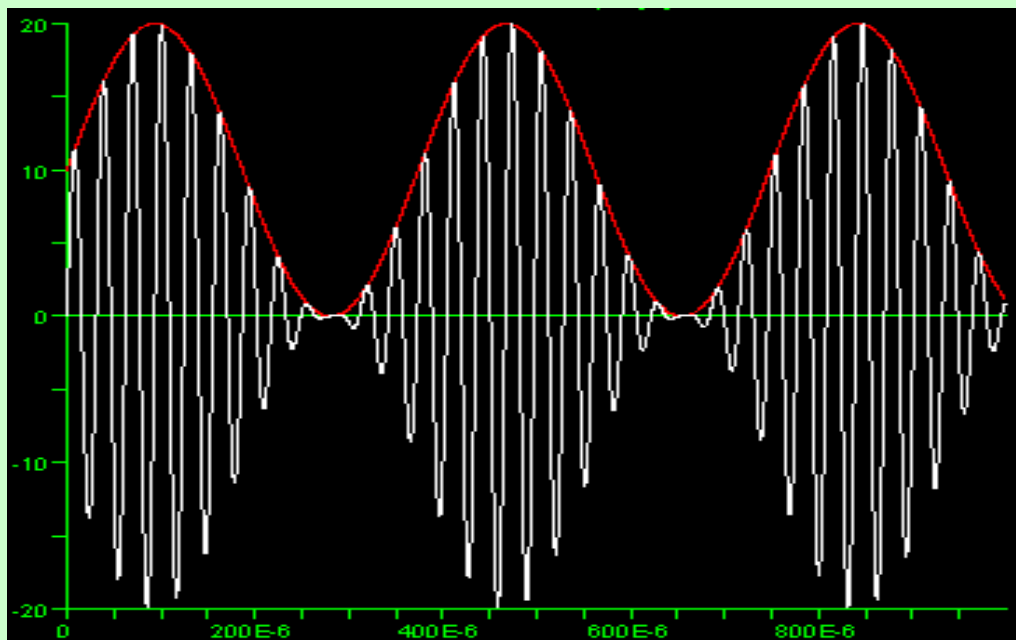


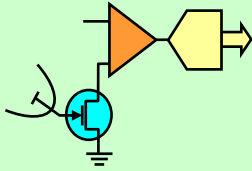
spectrum



AM modulation; $m = 1$

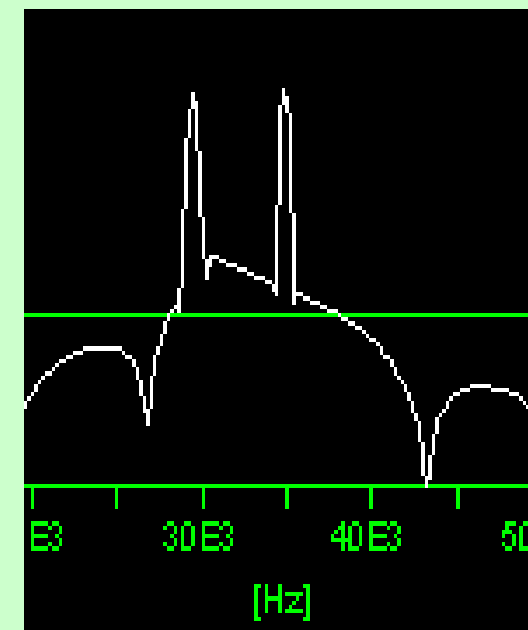
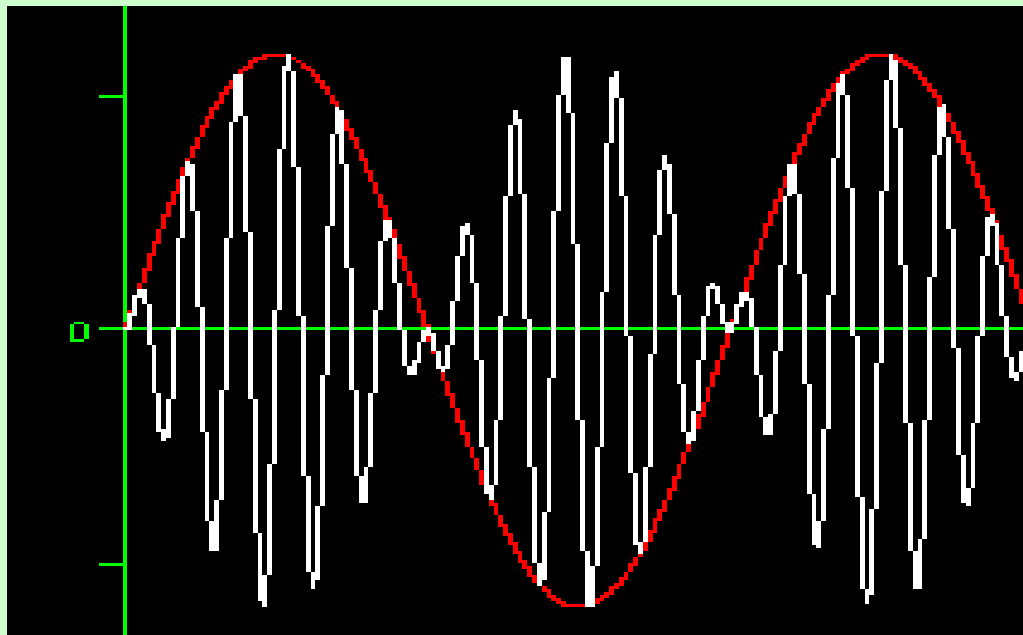
- $A = 10V$, $B = 10V$, $m = 1$ (100%)
 - the spectrum shows the carrier
 - Modulation signal \rightarrow envelope (red)

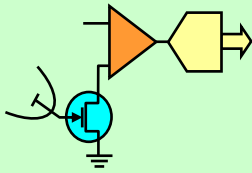




AM modulation - PSK

- $A = 10V$, $B = 0V$ (suppressed carrier, PSK/180°)
 - the carrier does not appear in the spectrum
 - Modulation signal \rightarrow envelope (red)

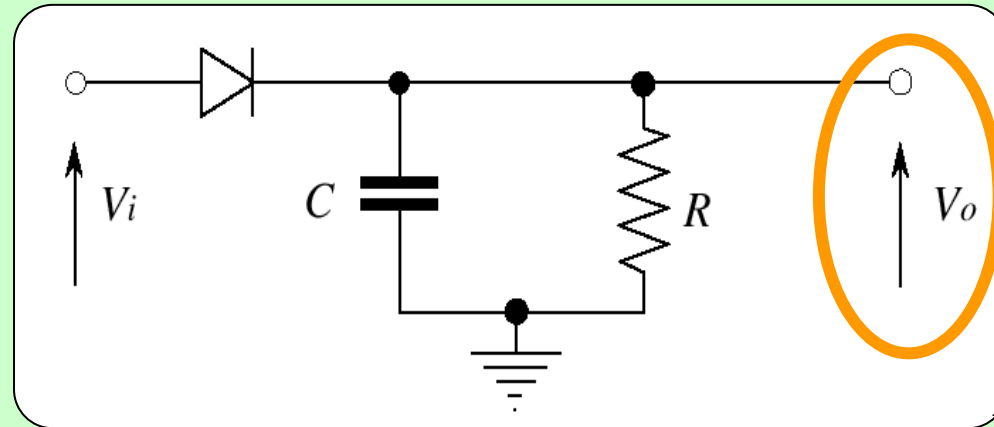




Envelope demodulator

- Peak detector with loss

- C charged to + peaks, discharged through R

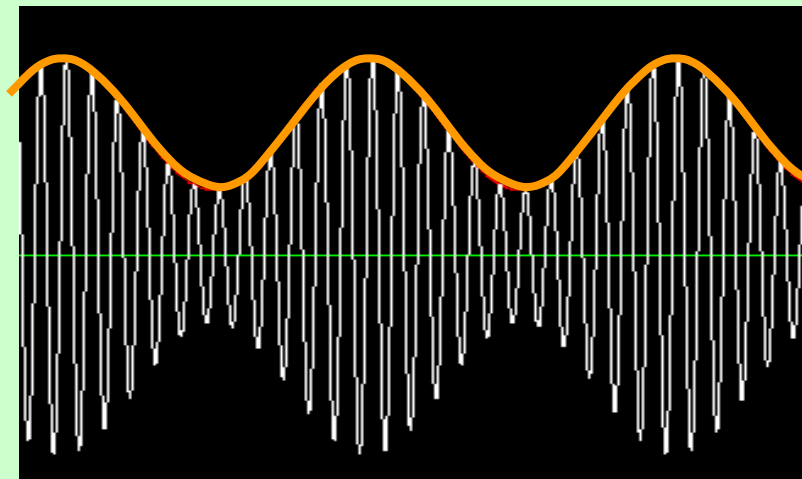


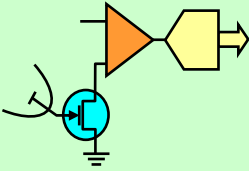
- Problems:

- Diode threshold
- Noise sensitivity
- Not for $M > 1$

- Improvements

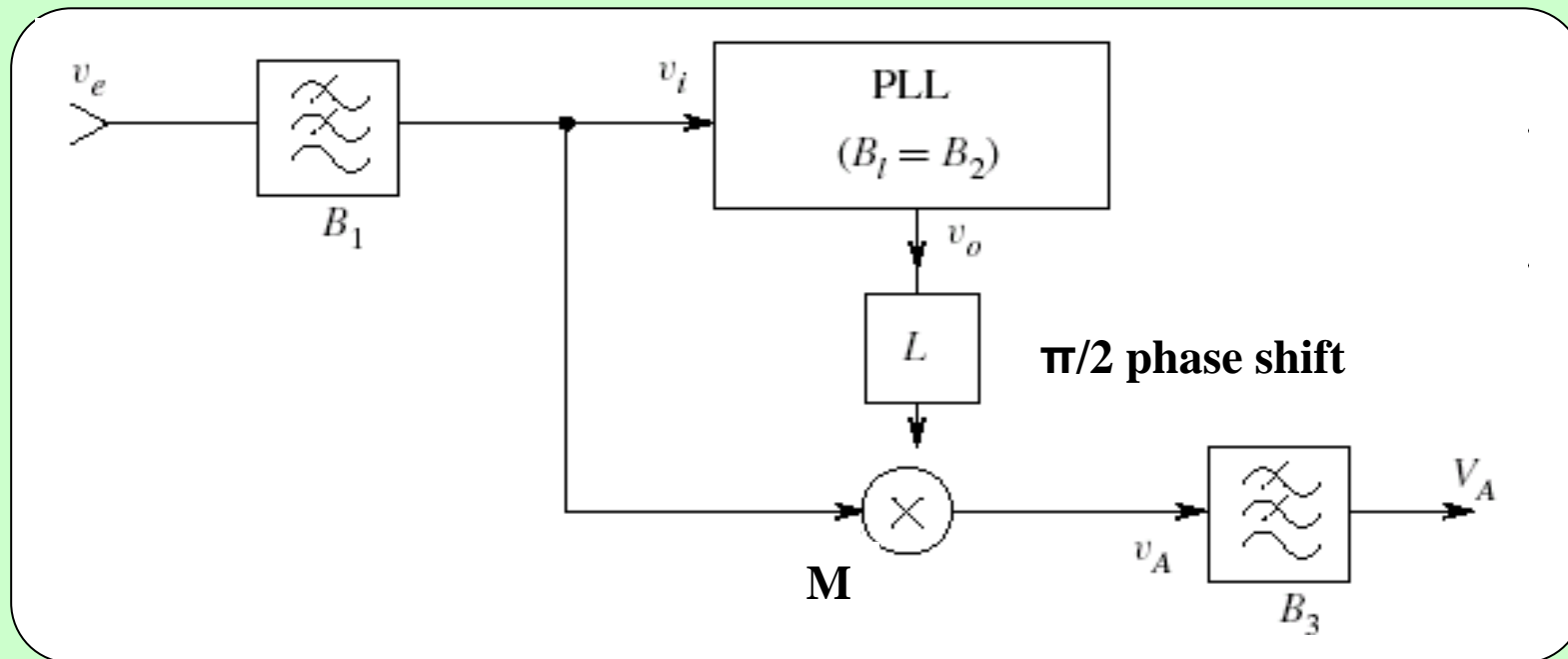
- Active diode
- Full wave rectifier

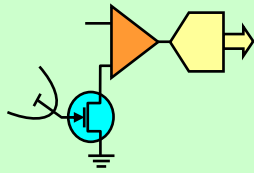




Coherent demodulation

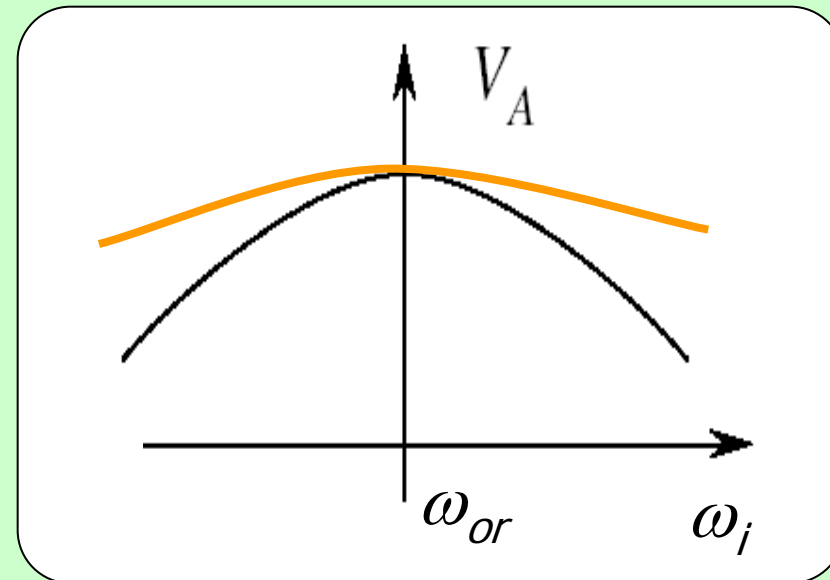
- B_1 cuts outband noise
- The PLL generates the reference signal
- The multiplier M moves V_i to baseband
- B_3 isolates baseband signal

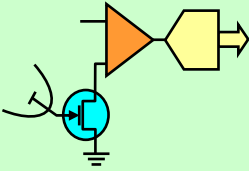




Effect of frequency drift

- Changes in F_i cause phase error in the PLL
 - To move the VCO: $V_c \neq 0$
 - To get $V_c \neq 0$: $\theta_e \neq 0$
 - Output error related with $\cos \theta_e$
 - Cross-demodulation (from FM to AM)
- To reduce the error
 - Increase loop gain
 - I/Q demodulator

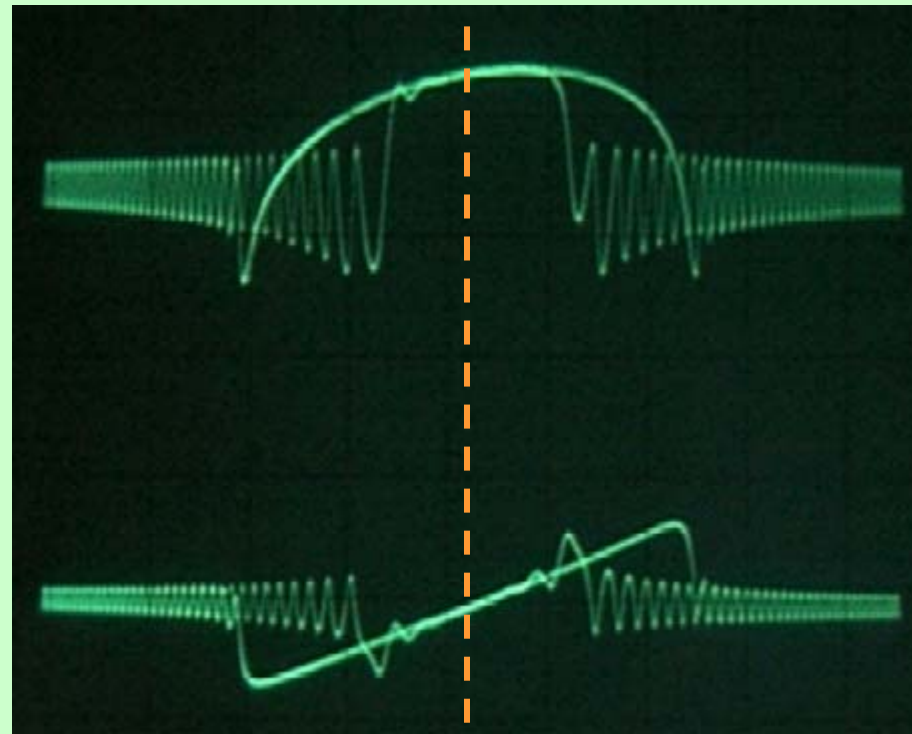




AM demodulator output vs frequency

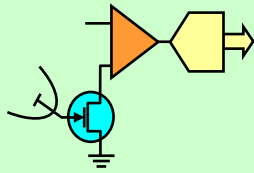
AM demod output

VCO control (Vc)



ω_{or}

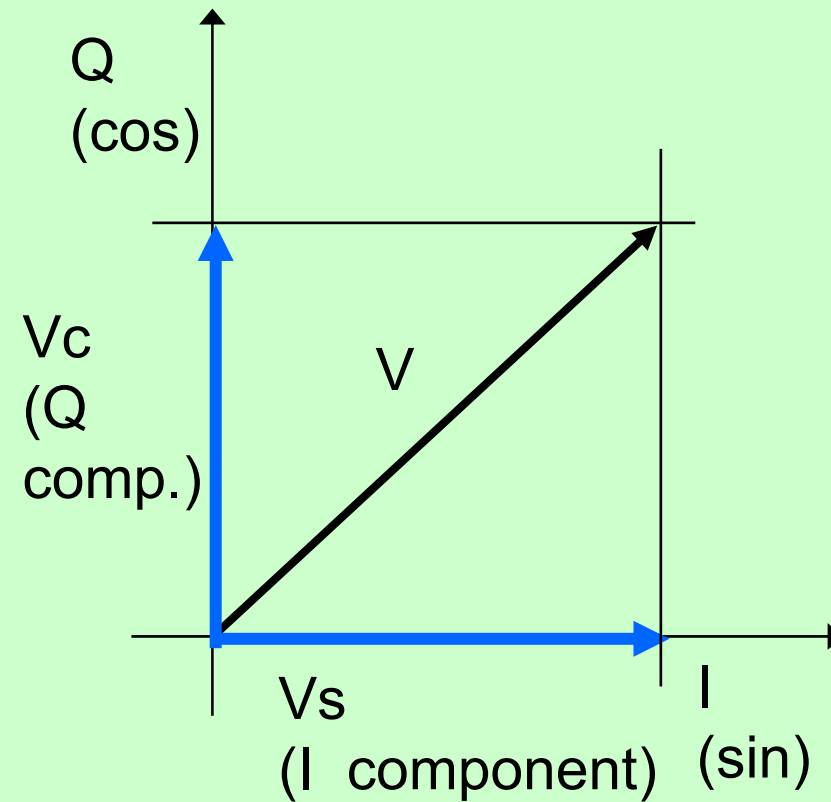
ω_i, ω_o

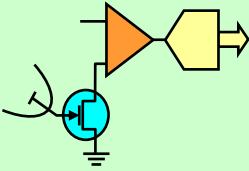


I-Q demodulation

$$\begin{cases} V_C = \vec{V} \times \cos \omega t \\ V_S = \vec{V} \times \sin \omega t \end{cases}$$

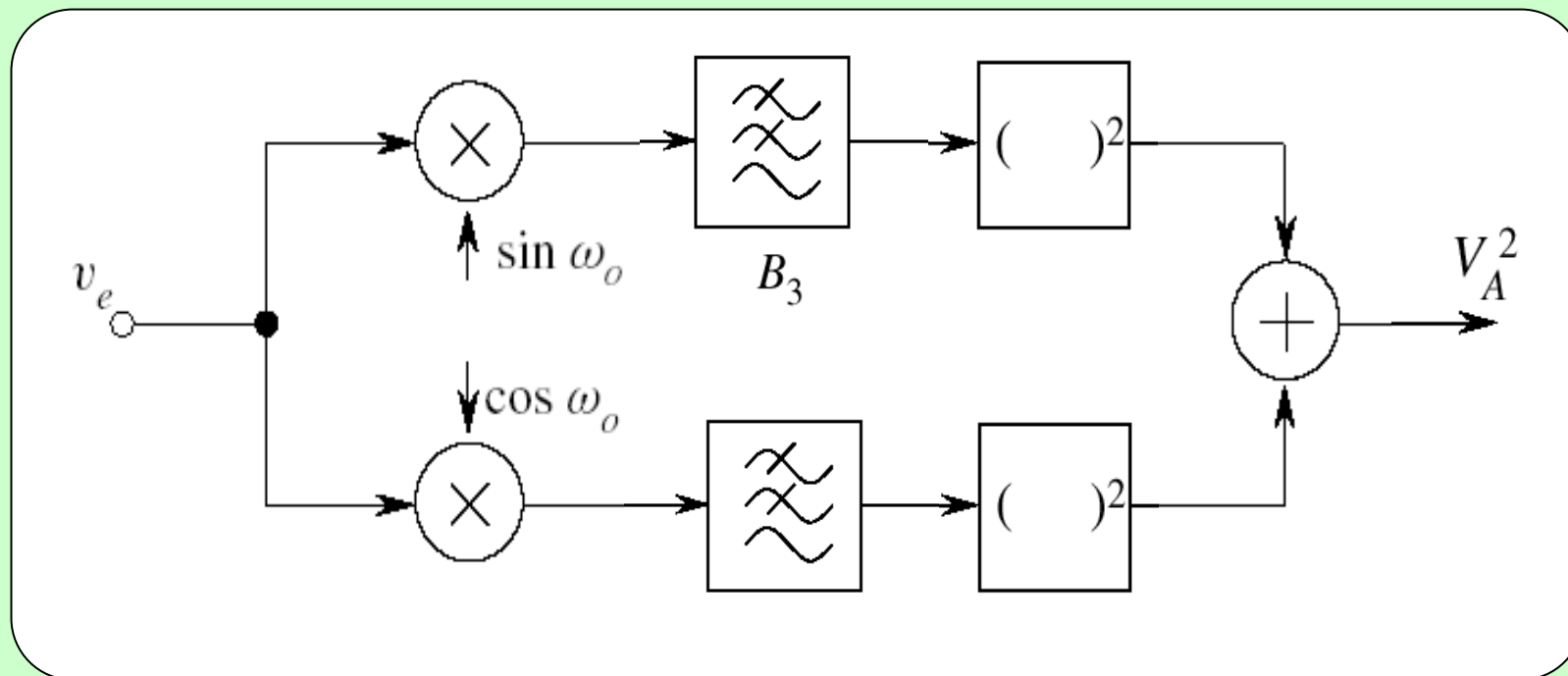
$$|\vec{V}| = \sqrt{V_C^2 + V_S^2}$$

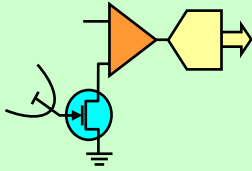




Analog I-Q demodulation

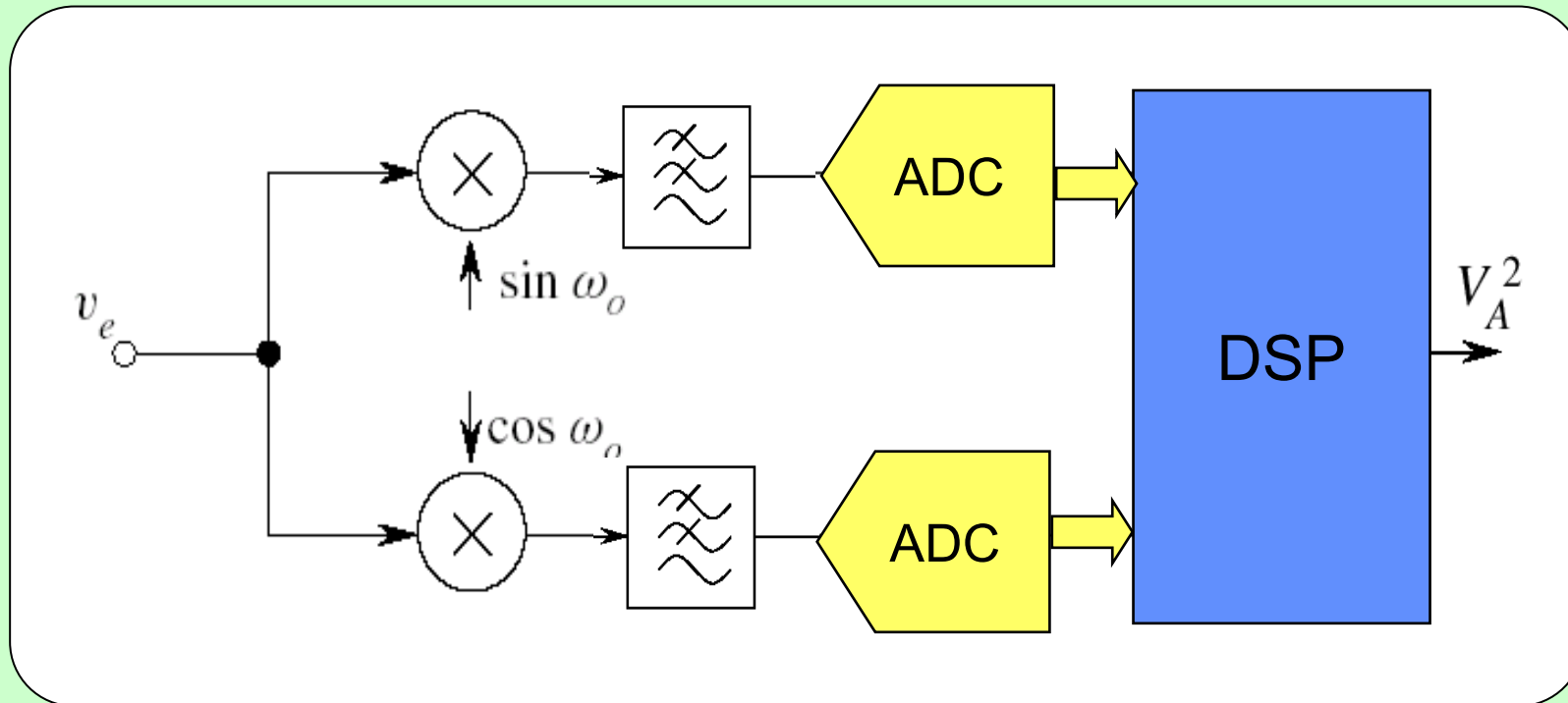
- Independent I-Q amplitude demodulation
- V_a independent from $V_e - V_o$ phase relation

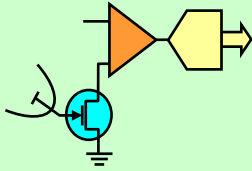




Digital I-Q demodulation

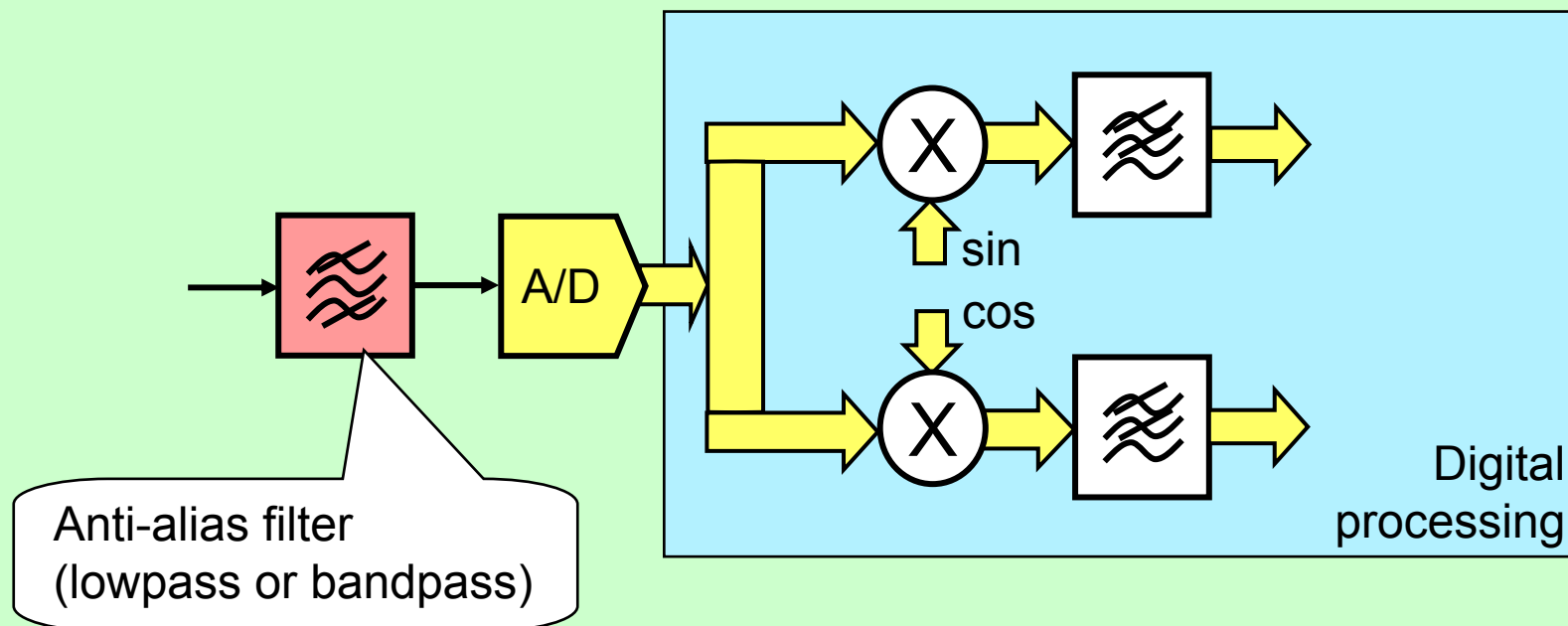
- A/D conversion after the multiplier (baseband)
- Digital processing

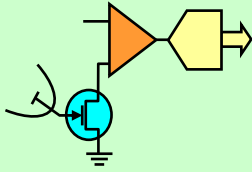




RF I-Q demodulation

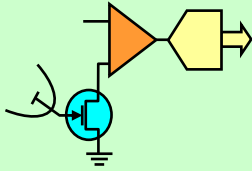
- Direct A/D conversion of RF signal
- Digital I/Q demodulation
- Digital processing





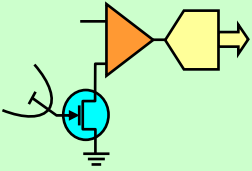
Lesson C5: synchronous demod.

- FM demodulators
- AM demodulators
 - Envelope demodulators
 - Synchronous demodulators
- Digital modulations
 - FSK, PSK, ASK and others
- Tone decoders
 - NE 567 block diagram
 - Tone decoder parameters
- Lab experiment 5: tone decoder behavior



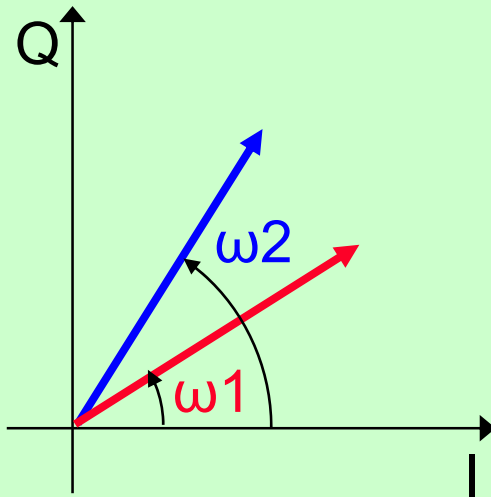
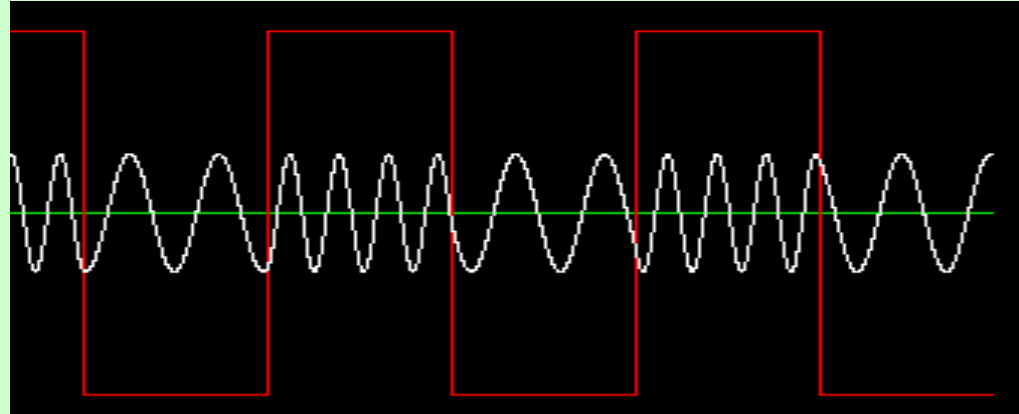
Digital modulations

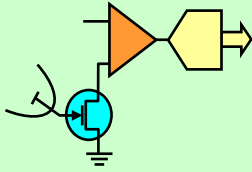
- ASK, PAM
 - Amplitude Shift Keyed
Pulse Amplitude Modulation
- FSK
 - Frequency Shift Keyed, FM to 2, ...N frequencies
- PSK
 - Phase Shift Keyed, PM to 2, ...N phases
- Mixed, QAM
 - ...



FSK signal

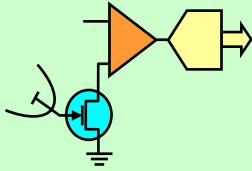
- FSK
frequency
shift keyed





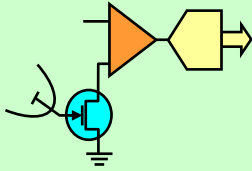
Digital FM → FSK

- Same techniques as analog FM
 - The transient response depends on loop parameters
- Separate AM channels for each carrier
 - Tone decoders with WTA



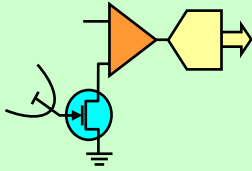
FSK Demodulators

- Frequency Shift Keyed: FM to 2, ...N frequencies
- Demodulation techniques
 - Single PLL, always locked \rightarrow output = V_c
 - Multiple coherent AM detector
 - » For each frequency PLL + AM coherent demodulators
 - » output comparison (WTA)
 - Multiple envelope detector
 - » Passband filter bank + envelope demodulators
 - » output comparison (WTA)
- Tradeoff for all circuits (symbol passband filters)
 - Wideband: fast response, noise-sensitive
 - Narrowband: slow response (good if Bitrate < carrier/10)



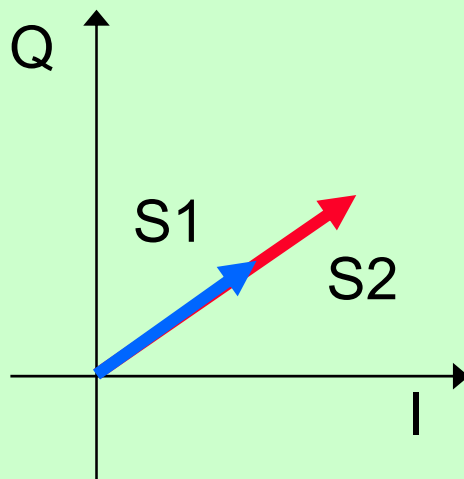
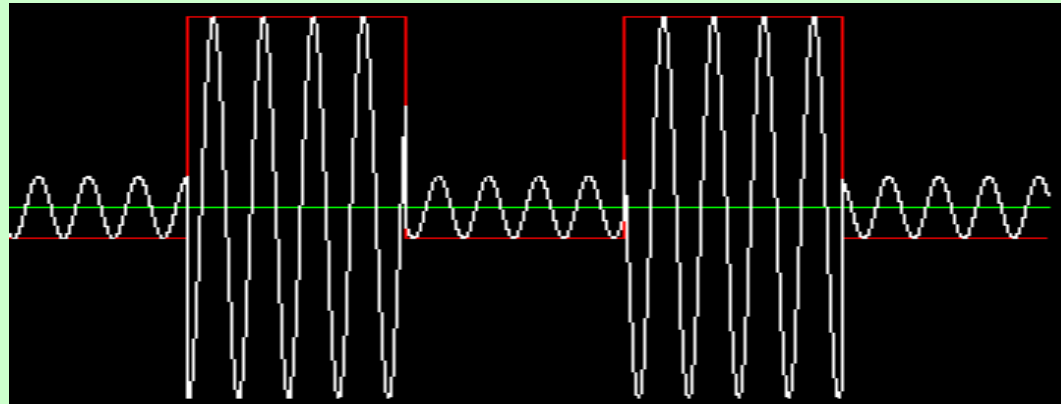
PAM/ASK demodulators

- Pulse Amplitude Modulation (PAM) or Amplitude Shift Keyed (ASK)
 - Discrete AM (2, ...N levels)
- Demodulation techniques
 - Envelope detector
 - Coherent demodulation (PLL)
 - + output comparison (WTA)
- Tradeoff for all circuits: post-detection filter
 - Wideband : fast response, noise-sensitive
 - Narrowband: slow response

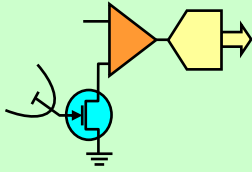


ASK signal

- ASK (PAM) discrete amplitude change

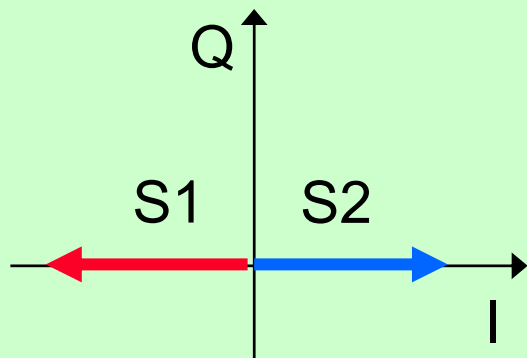
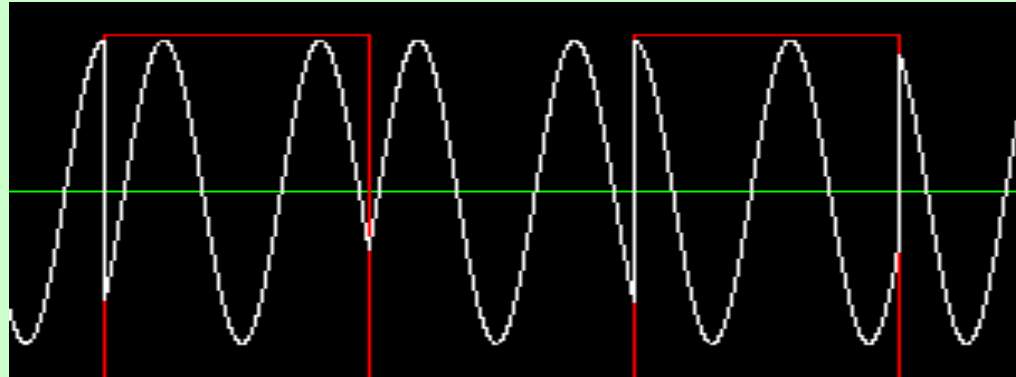


2-level ASK

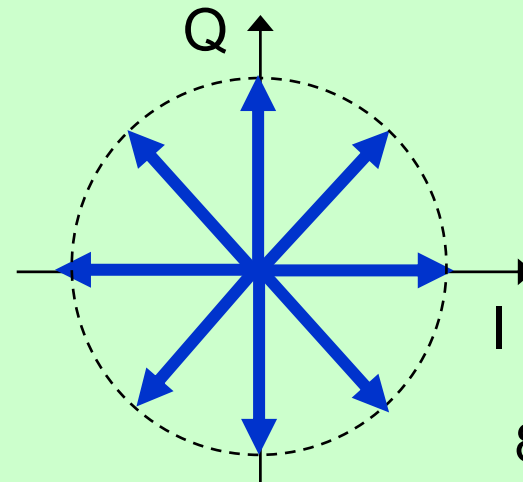


PSK signal

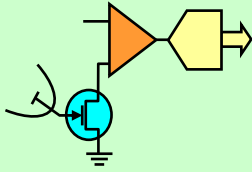
- PSK phase shift



2-phase
(rotation π)

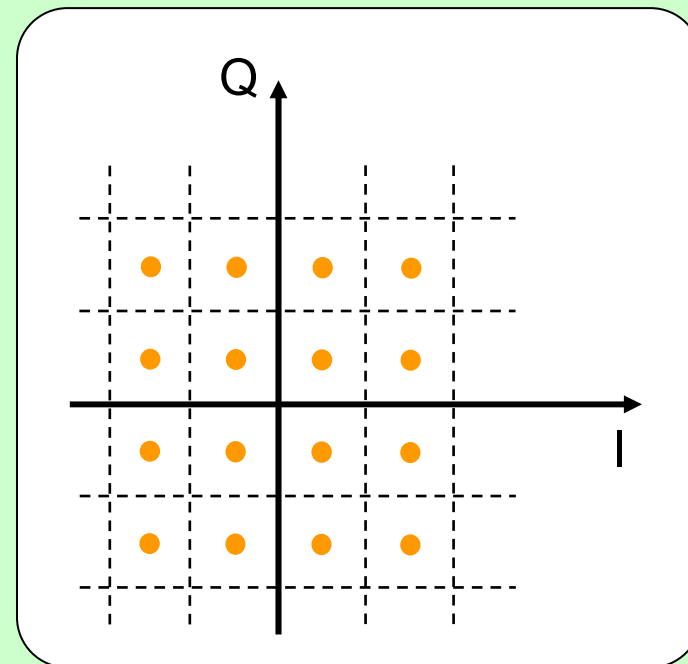


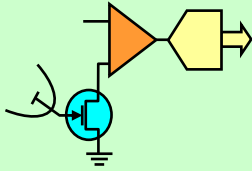
8-phase
(rotation $\pi/4$)



Complex signal (ASK+PSK)

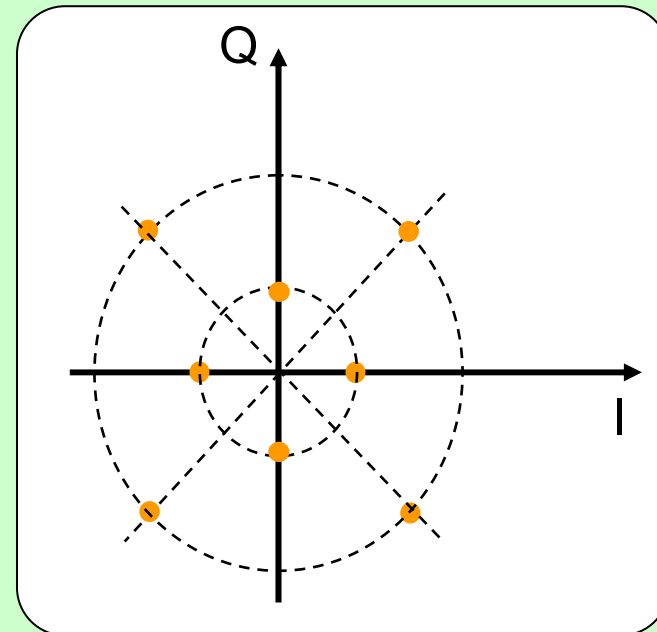
- Amplitude and phase discrete changes
 - QAM
 - Signal constellation
- Example with 16 symbols
 - In the I/Q plane can be seen as combinations of
 - 4 possible I values
 - 4 possible Q values

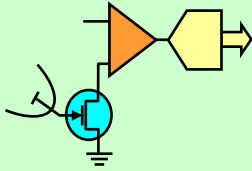




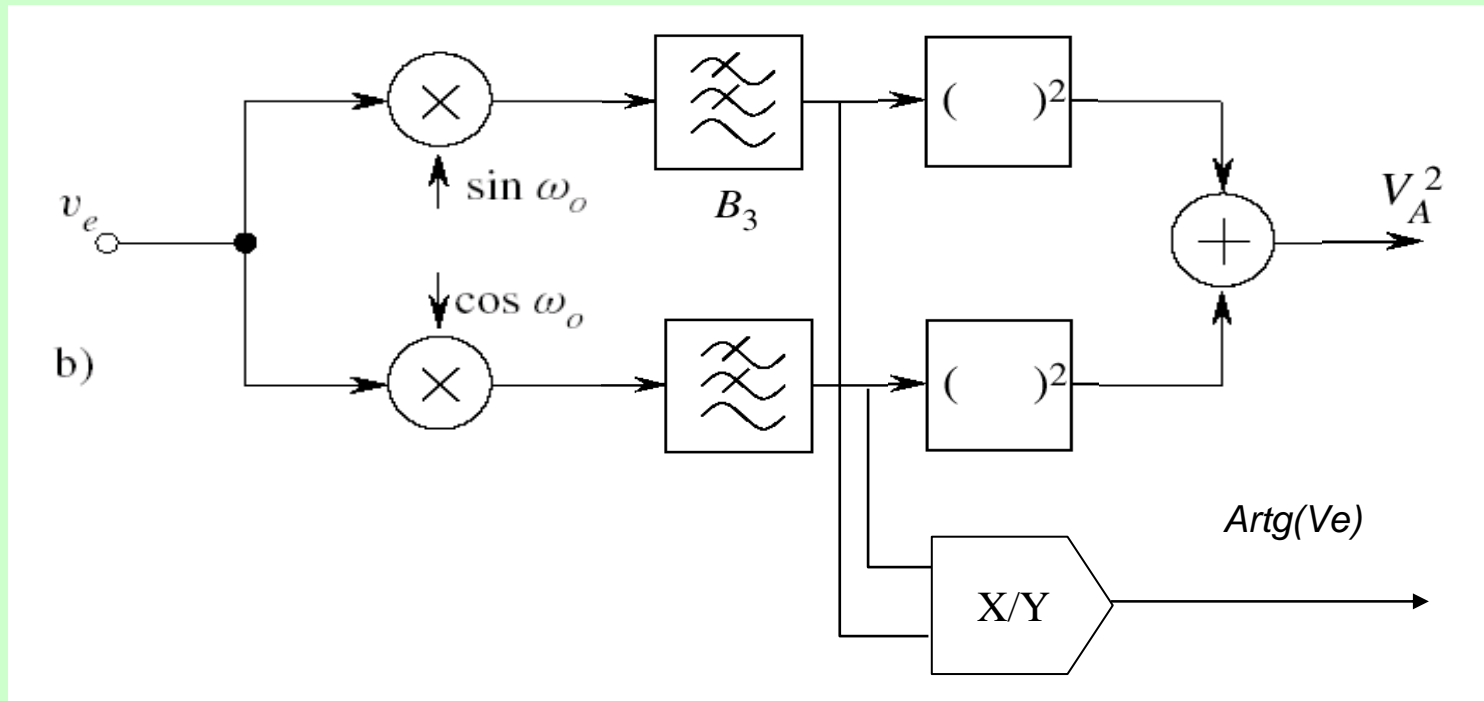
Complex signals demodulation

- Example 2
 - Phase shift: $\pi/2$
(4 states)
 - Amplitude levels 2
 - 3 bit/symbol
- In both cases:
- I/Q demodulation
- The I/Q components are obtained by coherent demodulation



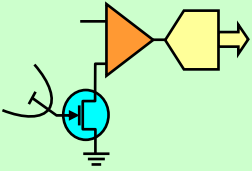


I/Q demodulation: A/P components

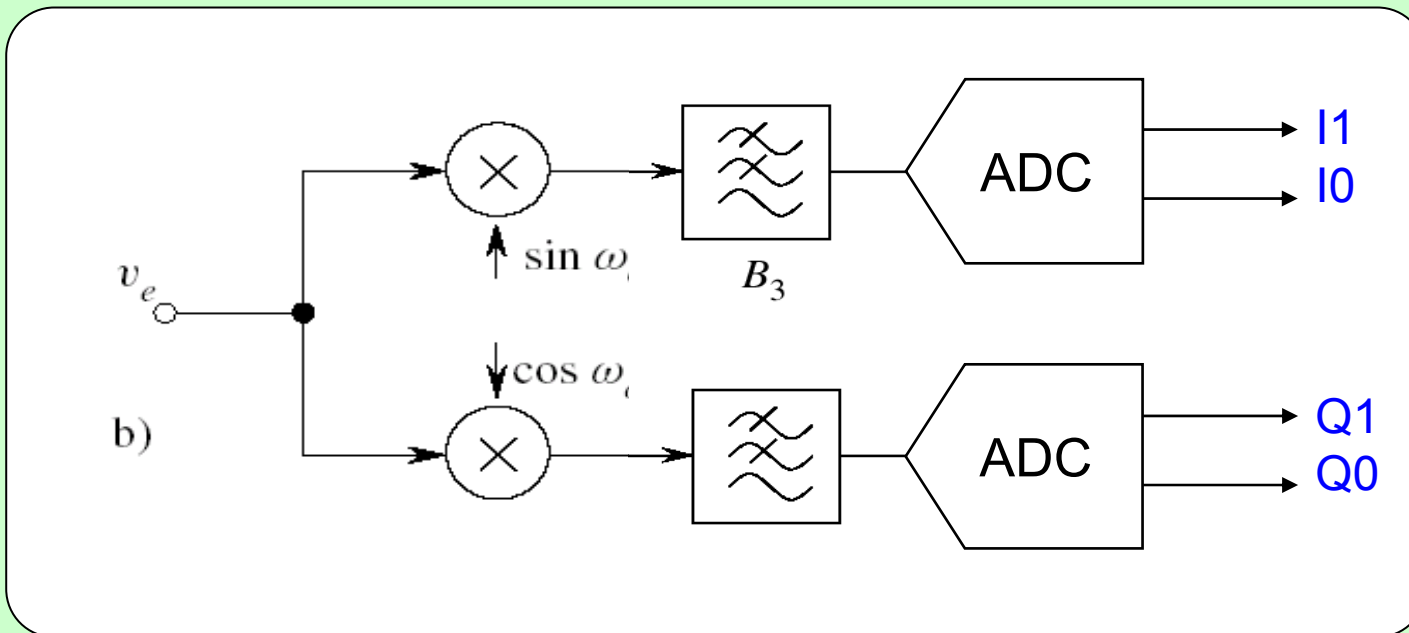


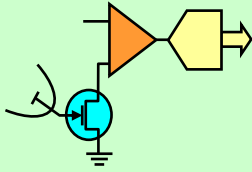
$$\begin{cases} V_C = \vec{V} \times \cos \omega t \\ V_S = \vec{V} \times \sin \omega t \end{cases}$$

$$\begin{cases} |\vec{V}| = \sqrt{V_C^2 + V_S^2} \\ \angle \vec{V} = \arctg \frac{V_S}{V_C} \end{cases}$$



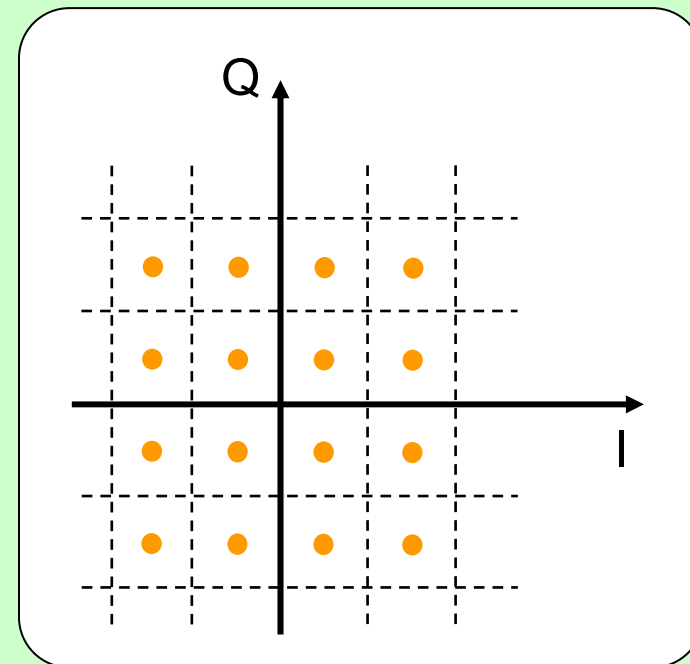
I/Q demodulation: I/Q components

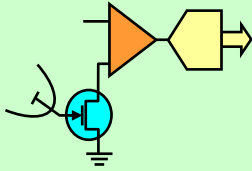




Complex signal (ASK+PSK)

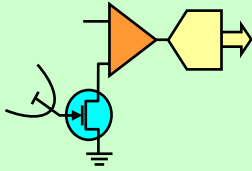
- Amplitude and phase discrete changes
 - QAM
 - Signal constellation
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 - 4 possible Q values





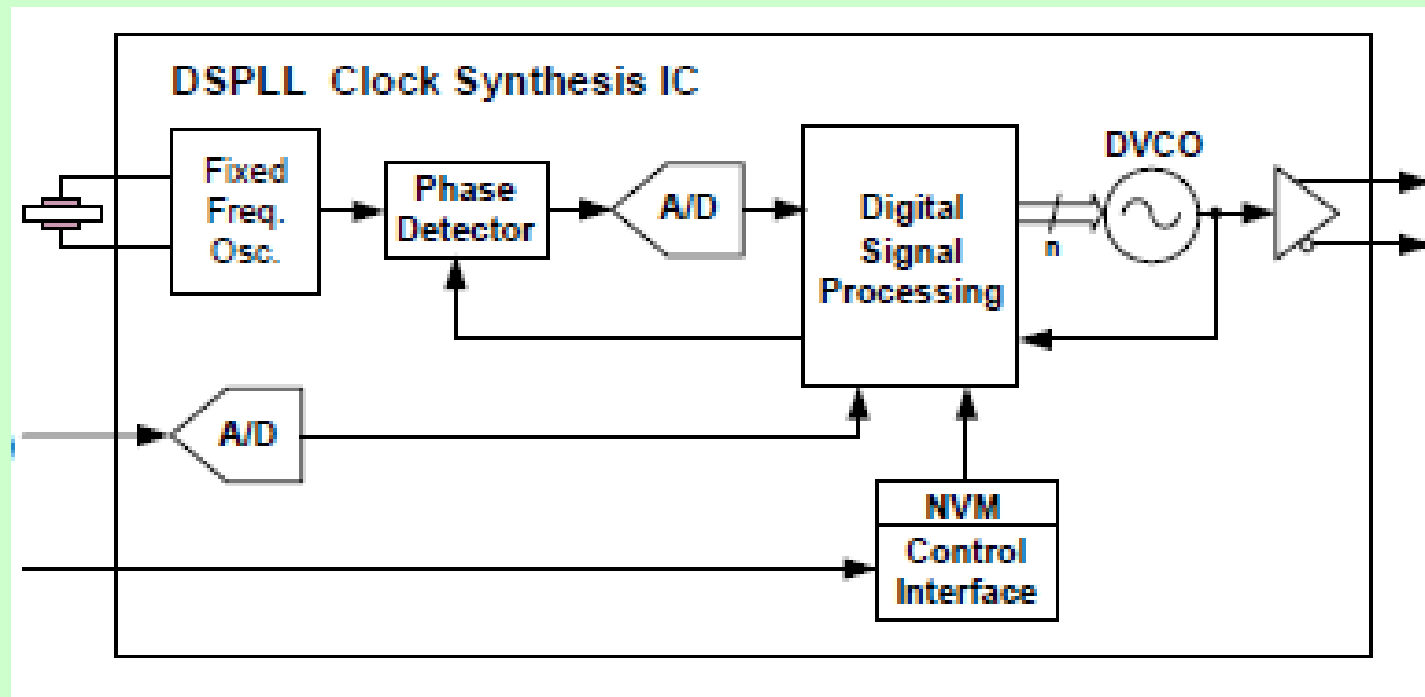
The ADPLL

- PLL based on digital circuits
 - Wired logic
 - Programmable logic
 - Processor + SW \rightarrow DSPLL
- Programmable parameters, with better control
- Digital $V_i \rightarrow$ ADC on V_d
 - Digital loop filter + Numeric Controlled Oscillator
- Analog $V_i \rightarrow$ ADC on V_i
 - Digital PD + Digital loop filter + NCO

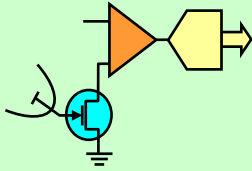


Example of DSP-PLL: Si550

- Variable frequency clock generator
 - Analog PD, then ADC
 - 10 MHz – 1,4 GHz range (Si550)

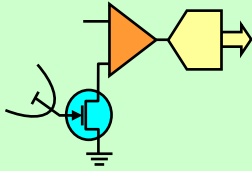


From <https://www.silabs.com>



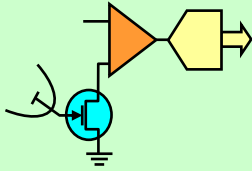
Lesson C5: synchronous demod.

- FM demodulators
- AM demodulators
 - Envelope demodulators
 - Synchronous demodulators
- Digital modulations
 - FSK, PSK, ASK and others
- Tone decoders
 - NE 567 block diagram and parameters



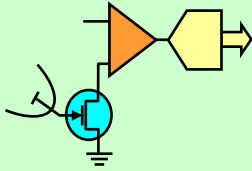
Integrated Tone Decoder

- NE567, LM576, ...: bipolar / LMC567: CMOS
 - Same function, slightly different structures
- Tone decoder operation:
 - Recognize a carrier (tone) within a frequency interval, even with strong interferences by noise and other signals
 - Used to recognize commands, numbers (phone), signalling overlapped with other signals
- Structure
 - PLL for analog signals + AM synchronous demodulator
- Features
 - Very narrow bandwidth
 - ON/OFF output + intermediate analog output



Tone decoder: specs

- Frequency range
 - Allowed values for the tone to be recognized
- Bandwidth
 - Frequency window for decoding of the tone
- Input amplitude range
 - Maximum in-band input signal which is not recognized
 - Minimum in-band input signal which is recognized
- Noise and interferers
 - Allowed wideband noise
 - Allows narrowband interferers (other tones)

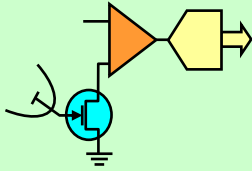


Tone decoder: bandwidth

- The device is designed to recognize a specific frequency, with minimum change
 - The PLL can lock only to a narrow frequency range
 - The possible shift of the VCO is minimum
- Detection bandwidth: about 15% of central frequency

Largest detection bandwidth	$f_0 = 100\text{kHz} = \frac{1}{1.1R_1C_1}$
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10	14	18	% of f_0
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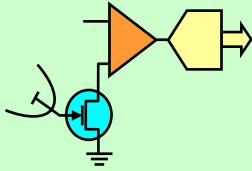


Tone decoder: input range

- Amplitude range for tone recognition

Smallest detectable input voltage ⁴		20	25	mV _{RMS}
Largest no-output input voltage ⁴	10	15		mV _{RMS}

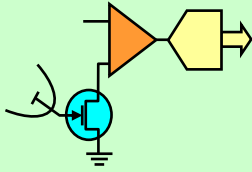
- Guaranteed minimum input level which is definitely recognized by the tone decoder (max of the min levels among several devices)
- Guaranteed maximum input level which is NOT recognized by the tone decoder (min of max levels)
- Same kind of specs as Vih/Vil for logic circuits



Tone decoder: noise and interferers

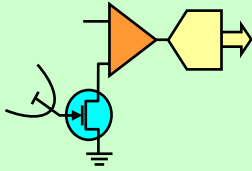
- Noise immunity
- Tone detection capability with noise or interferer stronger than the tone itself
 - (Outband signal)/(inband tone): + 6 dB
 - signal(tone)/(wideband noise): - 6 dB

Greatest simultaneous out-band signal-to-in-band signal ratio		+6		dB
Minimum input signal to wide-band noise ratio		-6		dB

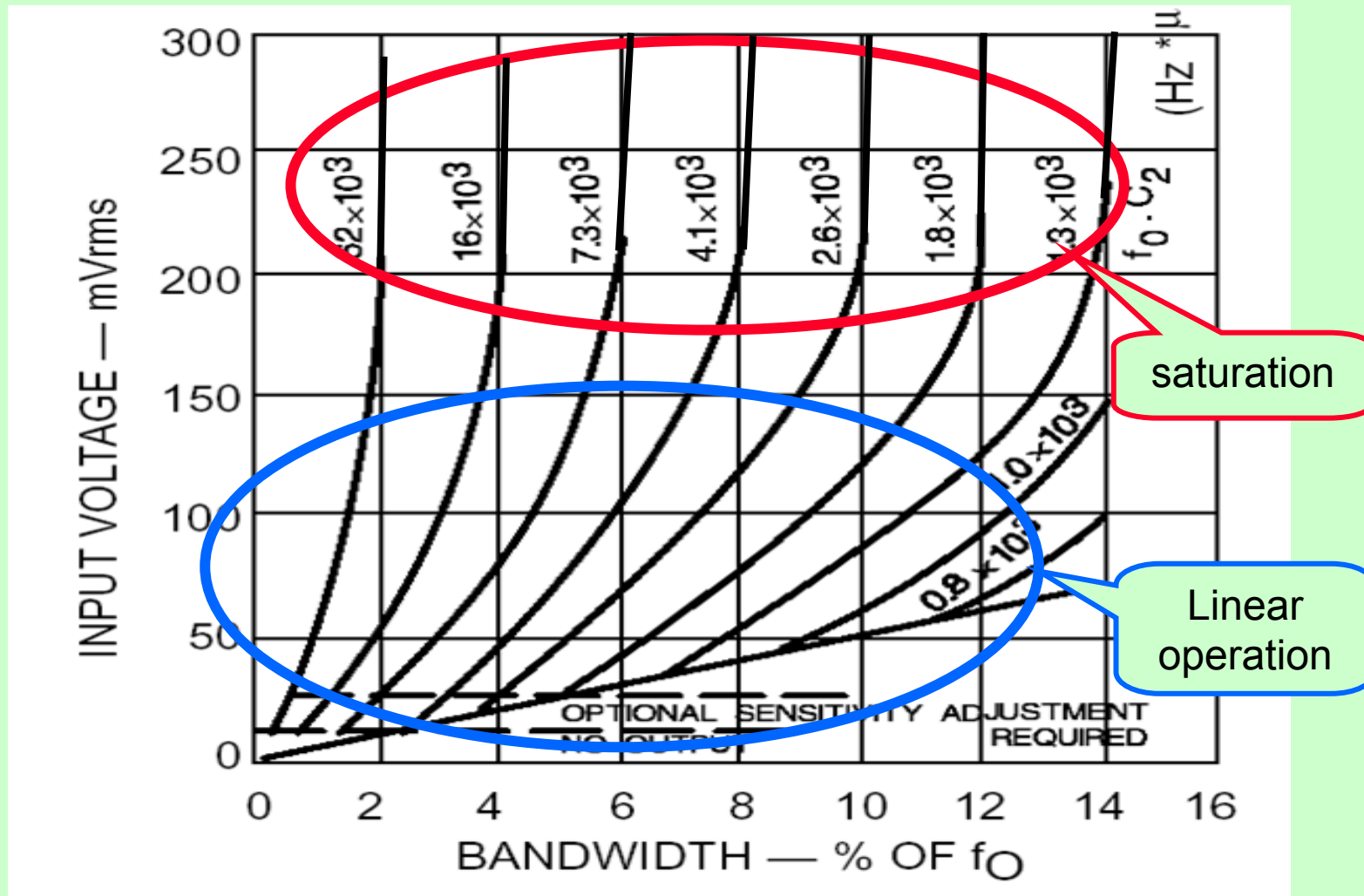


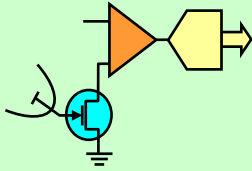
Tone decoder: bandwidth and $F(s)$

- The next diagram plots the capture range vs V_i and filter parameters
- Detection bandwidth (capture range) depends on:
 - Input level
 - Loop filter $F(s)$
- **Linear** area
 - $V_i < 100$ mV
 - Capture range depends on V_i
- **Saturation** area
 - $V_i > 200$ mV
 - Capture range does not depend on V_i

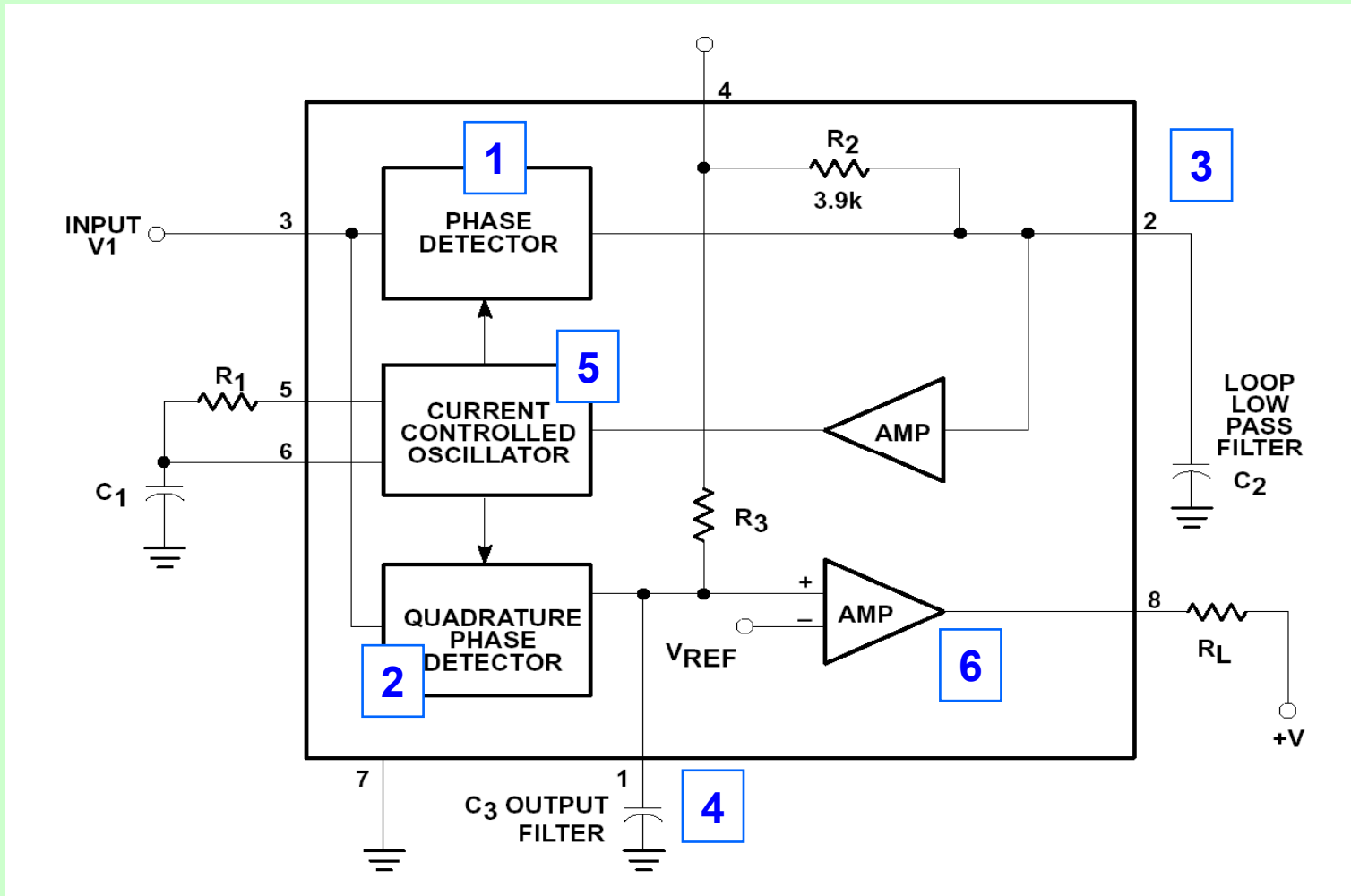


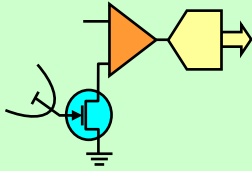
Linear and saturating input levels





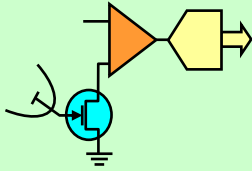
Tone decoder A: block diagram





Tone decoder functional units

1. Phase detector
2. Amplitude demodulator
 - Gilbert cell multiplier
3. Loop filter
4. AM filter
 - Single pole (RC), Internal R, external capacitor
5. VCO and I/Q outputs
 - C charge/discharge, threshold control
 - Third comparator or double frequency VCO
6. Output stage
 - open collector, high current capability (150 mA)



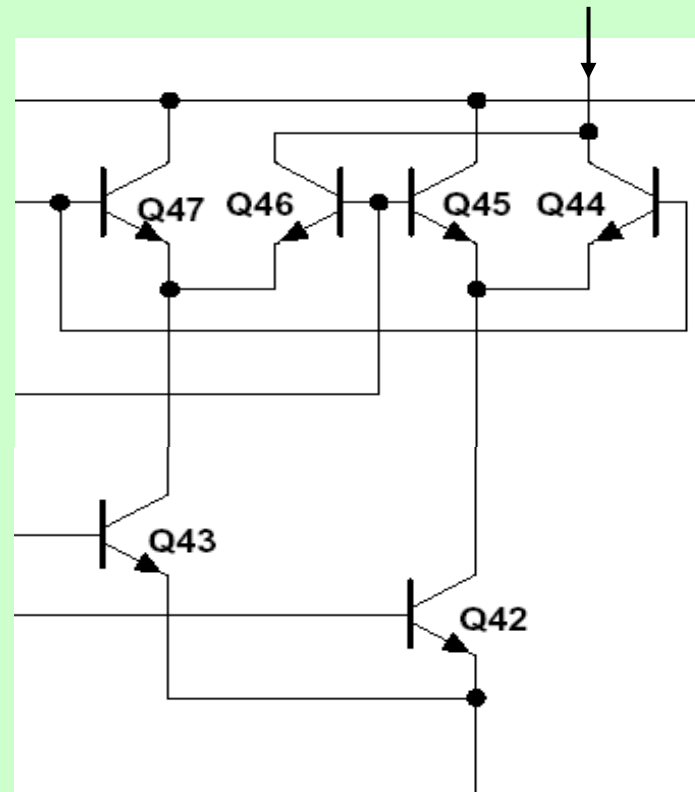
PD and AM demodulators

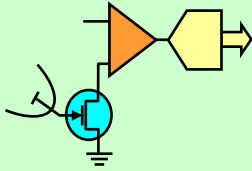
- Gilbert cell multipliers

Output I_z (current)

Input V_x

Input V_y





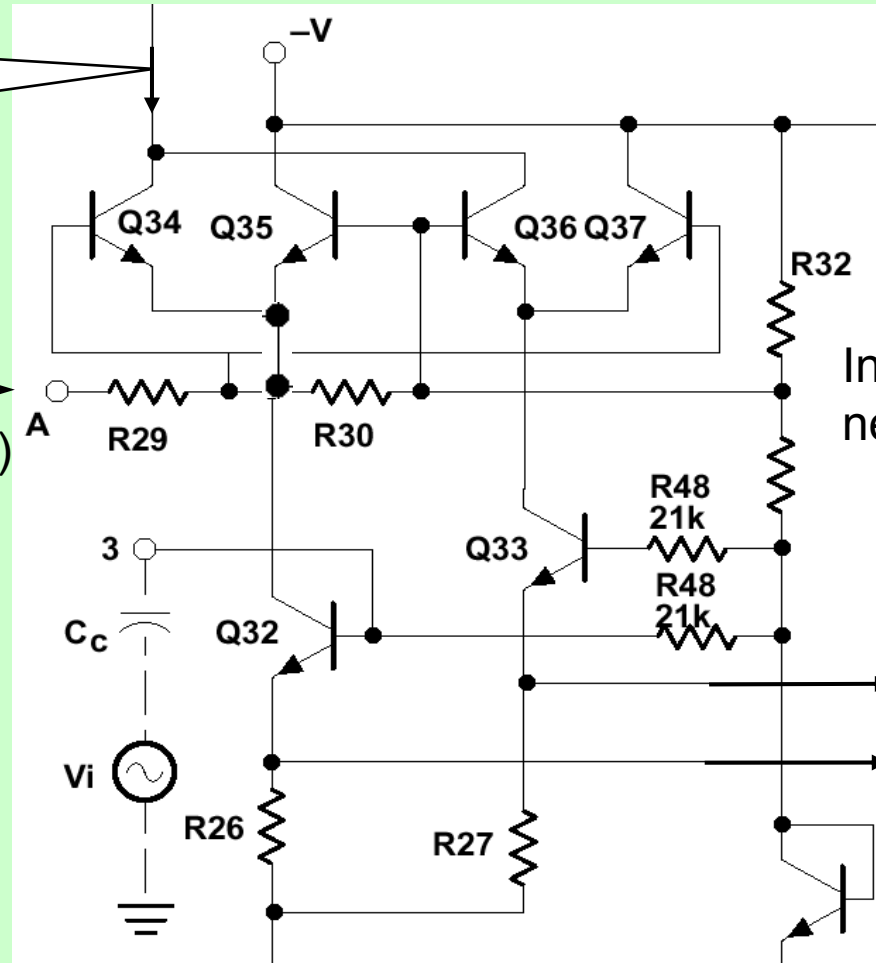
Linearization of differential stage

output I_z
(current)

V_x input
(V_o from VCO)

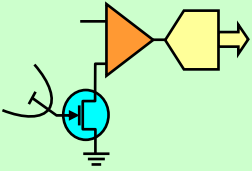
V_y input
(V_i signal)

R26, R27:
emitter feedback



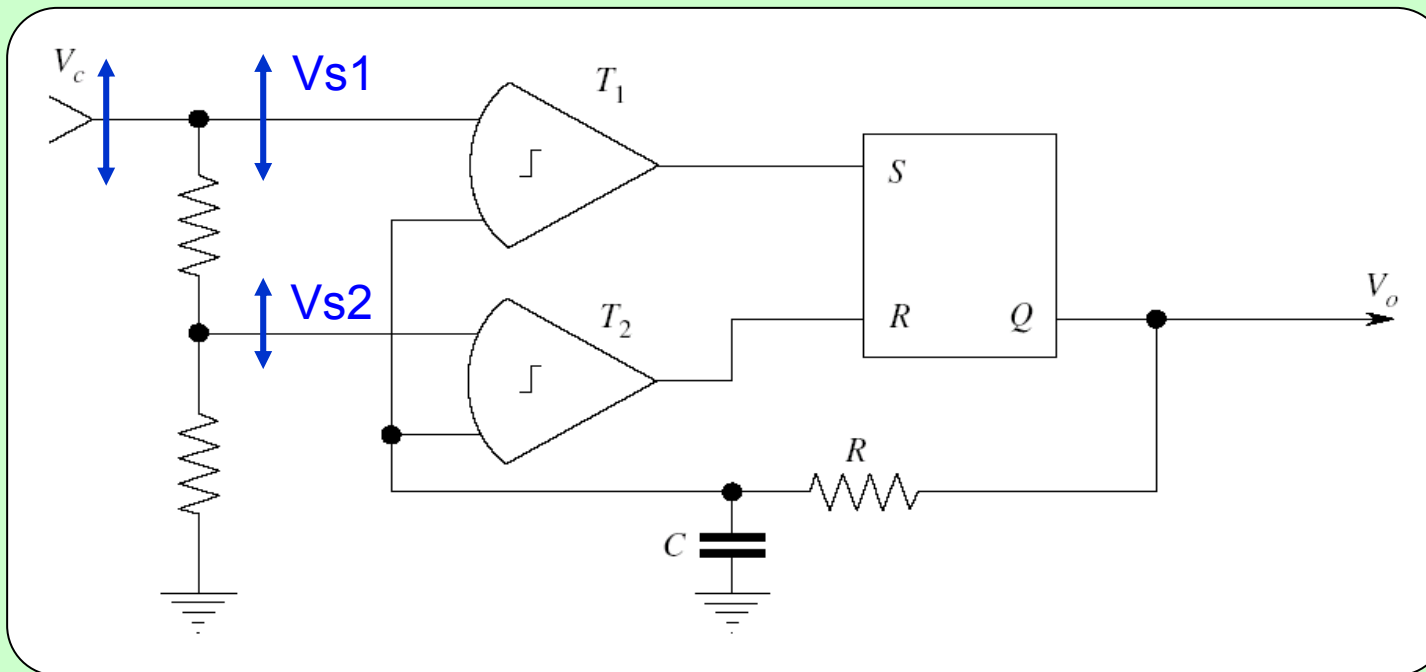
Input bias
network

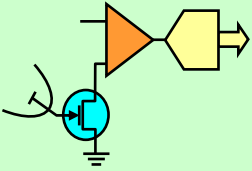
V_y input to AM
demodulator



I-C fixed τ VCO

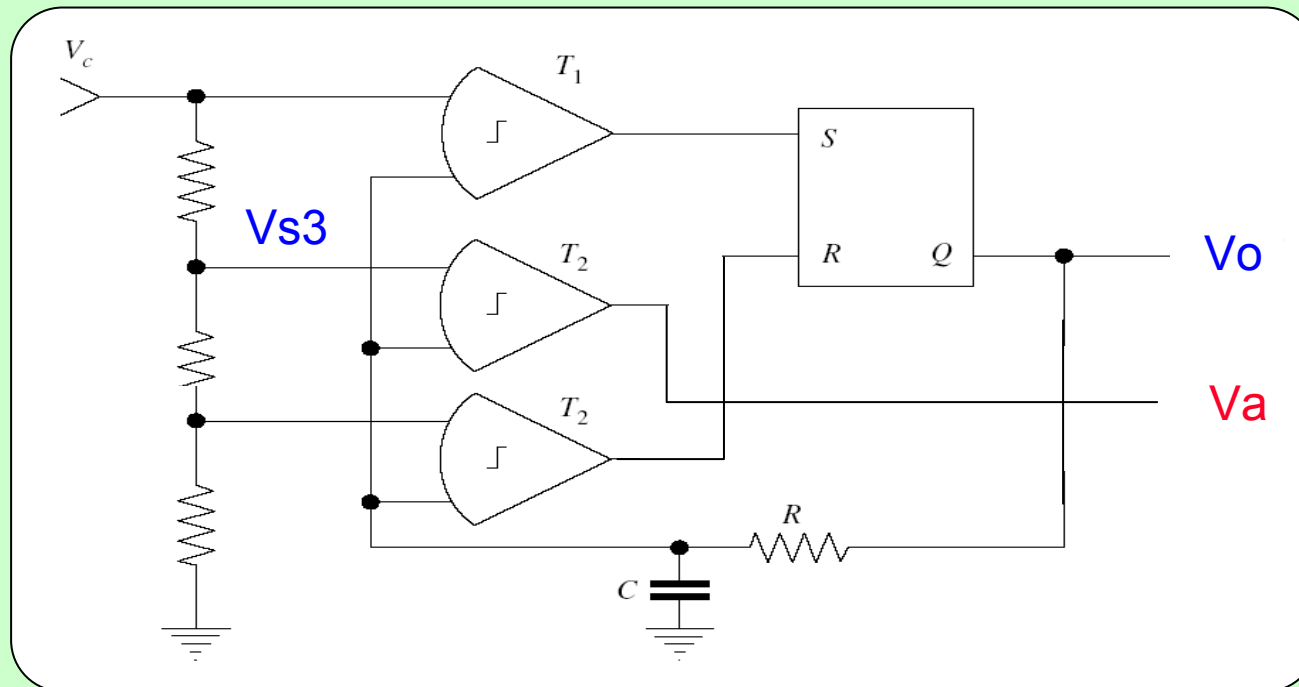
- Unique time constant ($\tau = RC$)
- Frequency control by **variable thresholds (V_{s1} , V_{s2})**
 - Limited frequency change

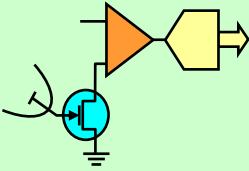




I/Q VCO outputs

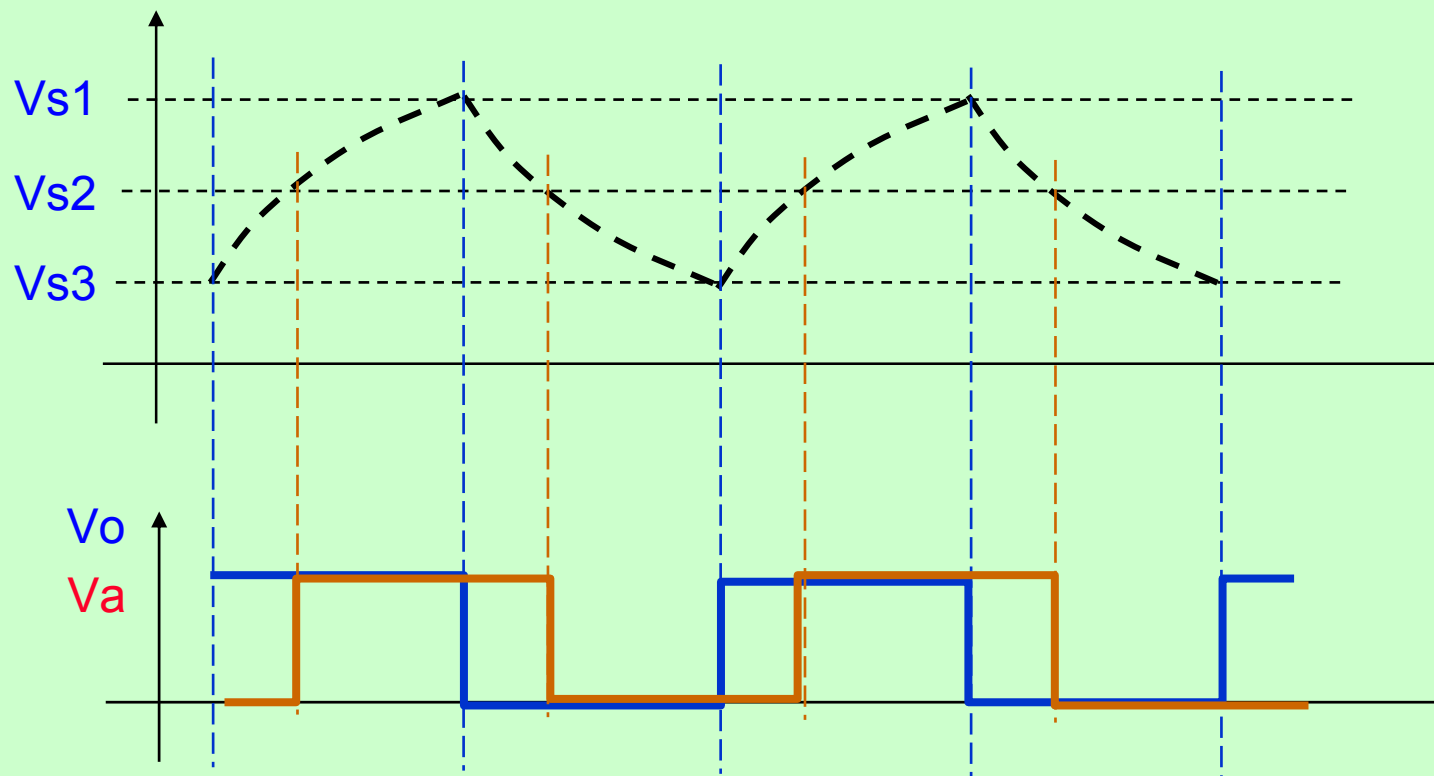
- Additional comparator on the capacitor voltage
 - Almost triangular waveform on C
 - Intermediate threshold V_{s3}

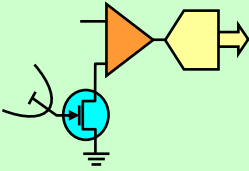




VCO waveforms

- Additional comparator on the capacitor voltage
 - Almost triangular waveform

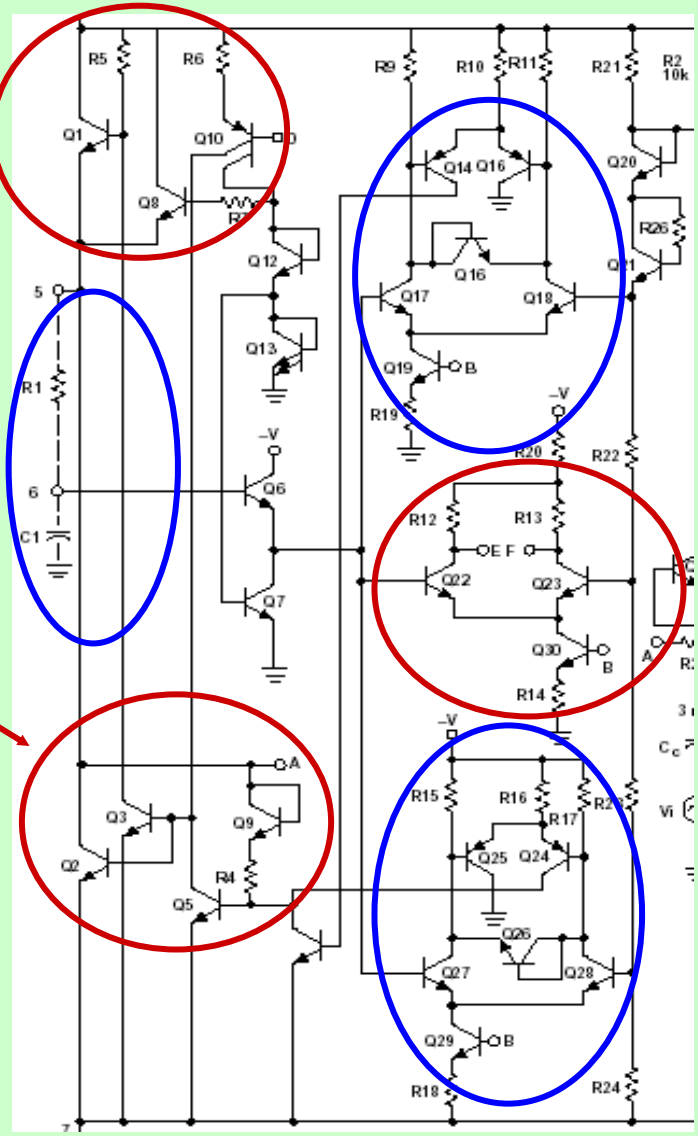




Tone decoder: VCO circuit

C charge/discharge switches

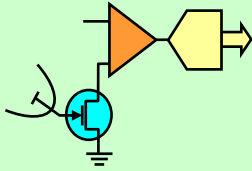
RC timing group



VCO Vs1 comparator

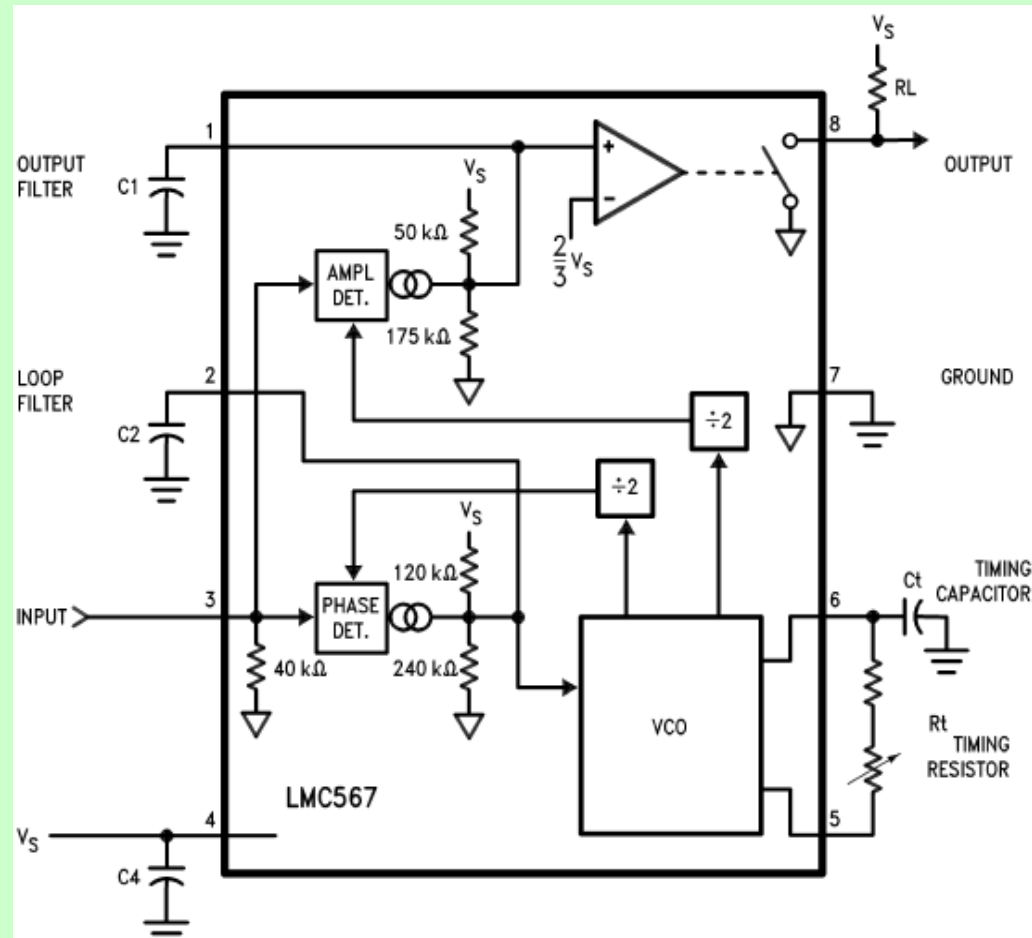
Q-output Comparator (Vs3)

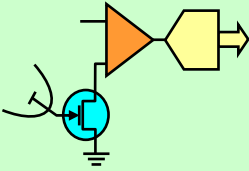
VCO Vs2 comparator



Tone decoder B: block diagram

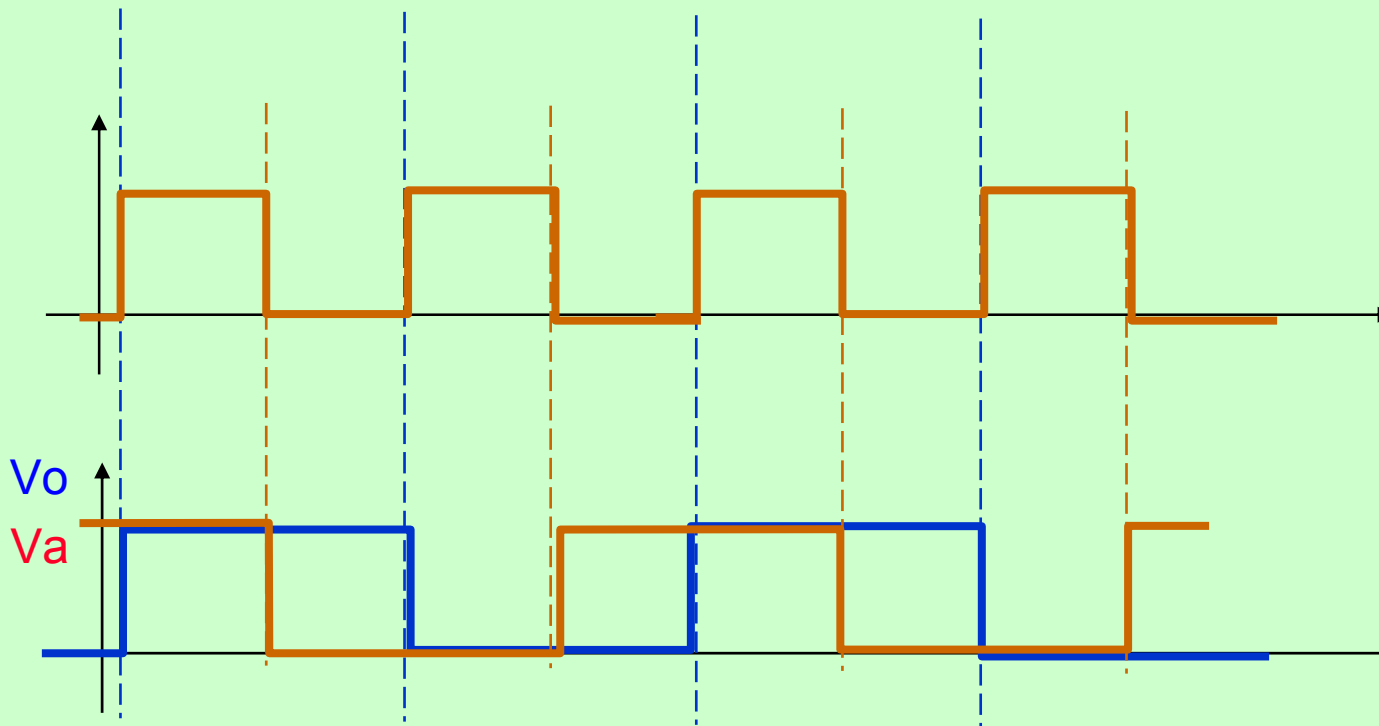
- CMOS features
 - Higher R/Z
 - Lower current
 - Better I/Q VCO

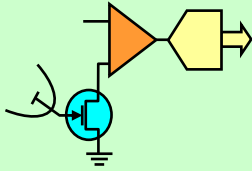




Double VCO frequency I/Q

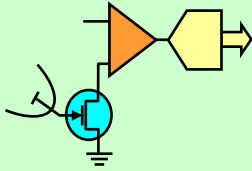
- VCO operates at double frequency
 - I/Q signals by Mod2 dividers on complementary edges





Lab experiment 4

- Design a circuit using the NE567 IC, to obtain a tone decoder with detection range centered on 25 kHz, and the maximum bandwidth allowed by the device.
- Build the circuit
- Verify the tone decoder parameters
 - Measure capture and lock ranges
 - Find the amplitude threshold (at central frequency)
 - Plot the VCO characteristic: $F_o(V_c)$
 - Plot the $V_a(F_i)$ and $V_a(V_i)$ characteristic
 - Verify the behaviour with noise and interferers at the input

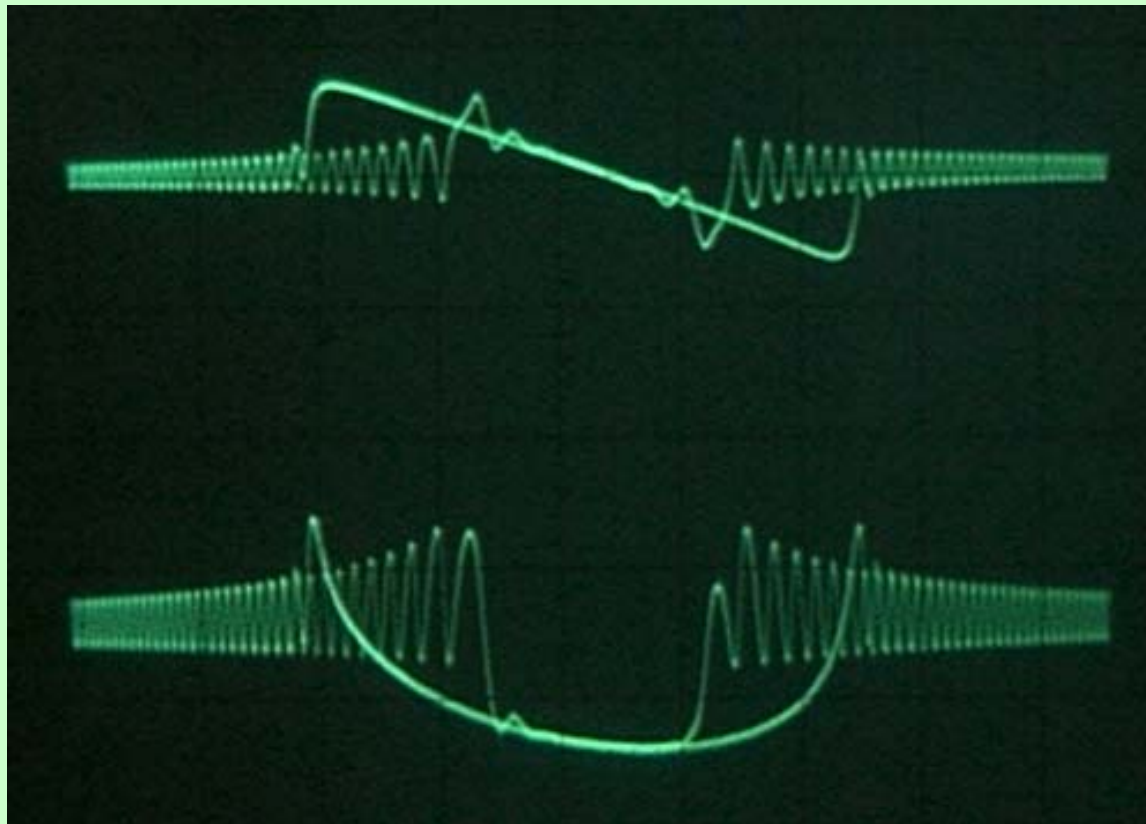


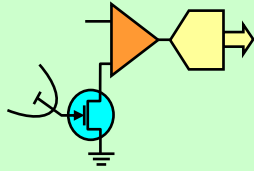
NE 576 – PD and AM demodulator

- PD and AM demodulator outputs vs input signal frequency.

VCO control
voltage
(butterfly plot)

Coherent AM
demodulator
output
(cosine shape)





Lesson C5

- Describe the techniques for FM demodulation, with and without PLL.
- Define the criteria to select R and C in the AM envelope detector.
- Which are the benefits of coherent AM demodulation vs envelope demodulation?
- How to reduce the FM sensitivity of an AM coherent demodulator ?
- List the parameters which describe the performance of a tone decoder.
- Propose some circuits to generate I/Q signals from a single VCO.